

SLUS822A-JUNE 2008-REVISED NOVEMBER 2008

UCC27200-Q1 UCC27201-Q1

## 120-V BOOT, 3-A PEAK, HIGH-FREQUENCY HIGH-SIDE/LOW-SIDE DRIVER

### **FEATURES**

- Qualified for Automotive Applications
- Specified from -40°C to 140°C
- Drives Two N-Channel MOSFETs in High-Side/Low-Side Configuration
- Maximum Boot Voltage 120 V
- Maximum V<sub>DD</sub> Voltage 20 V
- On-Chip 0.65-V VF, 0.6-Ω RD Bootstrap Diode
- Greater than 1 MHz of Operation
- 20-ns Propagation Delay Times
- 3-A Sink, 3-A Source Output Currents
- 8-ns Rise/7-ns Fall Time with 1000-pF Load
- 1-ns Delay Matching
- Undervoltage Lockout for High-Side and Low-Side Driver

### APPLICATIONS

- Power Supplies for Telecom, Datacom, and Merchant Markets
- Half-Bridge Applications and Full-Bridge Converters
- Isolated Bus Architecture
- Two-Switch Forward Converters
- Active-Clamp Forward Converters
- High-Voltage Synchronous-Buck Converters
- Class-D Audio Amplifiers

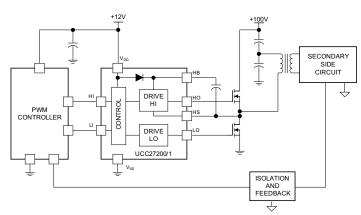
## DESCRIPTION

The UCC27200/1 family of high-frequency N-channel MOSFET drivers include a 120-V bootstrap diode and high-side/low-side driver with independent inputs for maximum control flexibility. This allows for N-channel MOSFET control in half-bridge, full-bridge, two-switch forward, and active clamp forward converters. The low-side and the high-side gate drivers are independently controlled and matched to 1 ns between the turn-on and turn-off of each other.

An on-chip bootstrap diode eliminates the external discrete diodes. Undervoltage lockout is provided for both the high-side and the low-side drivers, forcing the outputs low if the drive voltage is below the specified threshold.

Two versions of the UCC2720x are offered – the UCC27200 has high-noise-immune CMOS input thresholds, and the UCC27201 has TTL-compatible thresholds.

Both devices are offered in the 8-pin PowerPad<sup>™</sup> SOIC (DDA) package.



#### **Simplified Application Diagram**

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#### **ORDERING INFORMATION**<sup>(1)</sup>

Tj	INPUT COMPATIBILITY	PACKAG	E <sup>(2)</sup>	ORDERABLE PART NUMBER	TOP-SIDE MARKING	
-40°C to 140°C	CMOS	PowerPad – DDA	Reel of 2500	UCC27200QDDARQ1	27200Q	
-40 C 10 140 C	TTL	FOWEIFAU - DDA	Reel 01 2500	UCC27201QDDARQ1	27201Q	

For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI (1) web site at www.ti.com.

Package drawings, thermal data, and symbolization are available at www.ti.com/packaging. (2)

## ABSOLUTE MAXIMUM RATINGS<sup>(1)(2)</sup>

over operating free-air temperature (unless otherwise noted)

V <sub>DD</sub>	Supply voltage range		–0.3 V to 20 V
$V_{LI}, V_{HI}$	Input voltages on LI and HI		–0.3 V to 20 V
V		DC	–0.3 V to V <sub>DD</sub> + 0.3 V
V <sub>LO</sub>	Output voltage on LO	Repetitive pulse < 100 ns	-2 V to V <sub>DD</sub> + 0.3 V
		DC	$V_{\text{HS}}$ – 0.3 V to $V_{\text{HB}}$ + 0.3 V
V <sub>HO</sub> Output voltage on HO	Repetitive pulse < 100 ns	$V_{HS} - 2 V$ to $V_{HB} + 0.3 V$ , ( $V_{HB} - V_{HS} < 20$ )	
V		DC	-1 V to 120 V
V <sub>HS</sub>	HS voltage range	Repetitive pulse < 100 ns	–5 V to 120 V
V <sub>HB</sub>	HB voltage range		–0.3 V to 120 V
	HB-HS voltage range		–0.3 V to 20 V
TJ	Operating virtual-junction tem	perature range	–40°C to 150°C
T <sub>stg</sub>	Storage temperature range		–65°C to 150°C
T <sub>lead</sub>	Lead temperature	Soldering, 10 seconds	300°C
P <sub>D</sub>	Power dissipation	$T_A = 25^{\circ}C^{(3)}$	2.7 W

(1) Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

All voltages are with respect to V<sub>SS</sub>. Currents are positive into, negative out of the specified terminal. This data was taken using the JEDEC proposed high-K test PCB (See *Thermal Characteristics* for details). (2)

(3)

## **RECOMMENDED OPERATING CONDITIONS**

			MIN	NOM	MAX	UNIT	
V <sub>DD</sub>	Supply voltage range		8	12	17	V	
V	HS voltage	-1		105	.,		
V <sub>HS</sub>	HS voltage (repetitive pulse <100 ns)		-5		110	V	
V <sub>HB</sub>	HB voltage		V <sub>HS</sub> + 8, V <sub>DD</sub> – 1		V <sub>HS</sub> + 17, 115	V	
	Voltage slew rate on HS				50	V/ns	
TJ	Operating junction temperature	-40		140	°C		
<b>F0D</b>		Human-Body Model (HBM)		2000 1000		V	
ESD	Electrostatic discharge protection	Charged-Device Model (CDM)					



## THERMAL CHARACTERISTICS

over operating free-air temperature range, maximum power dissipation at ambient temperature:  $P_D = (150 - T_A)/\theta_{JA}$  (unless otherwise noted)

PACKAGE	θ <sub>JA</sub> (JUNCTION TO AMBIENT)	(JUNCTION TO CASE)	θ <sub>JP</sub> (JUNCTION TO THERMAL PAD)
DDA <sup>(1)</sup>	46°C/W	71°C/W	4.8°C/W

(1) Test board conditions:

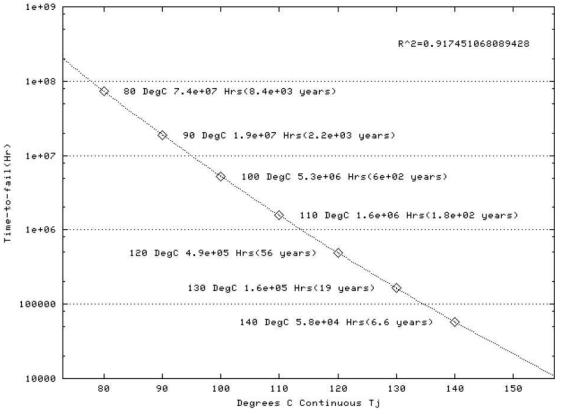
a. 3-in x 3-in, four layers, 0.062-in thickness

b. 2-oz copper traces located on the top and bottom of the PCB

c. 2-oz copper ground planes on the internal two layers

d. Six thermal vias in the PowerPad area under the device package

Wirebond Life for Mold Compound EME-G600(VENDOR DATA)







## **ELECTRICAL CHARACTERISTICS**

over operating free-air temperature range,  $V_{DD} = V_{HB} = 12$  V,  $V_{HS} = V_{SS} = 0$  V, No load on LO or HO,  $T_A = T_J = -40^{\circ}$ C to 140°C (unless otherwise noted)

	PARAMETER		TEST CONDITIONS			TYP	MAX	UNIT
Supply	Currents							
I <sub>DD</sub>	V <sub>DD</sub> quiescent current		$V_{LI} = V_{HI} = 0$			0.4	0.8	mA
	V <sub>DD</sub> operating current	UCC27200	$f = 500 \text{ kHz}, C_{1 \text{ OAD}} = 0$			2.5	4	mA
IDDO	UCC27201		$T = 500 \text{ KHZ}, \text{ C}_{LOAD} = 0$	0		3.8	5.5	ШA
I <sub>HB</sub>	Boot voltage quiescent current		$V_{LI} = V_{HI} = 0 V$			0.4	0.8	mA
I <sub>HBO</sub>	Boot voltage operating current		$f = 500 \text{ kHz}, C_{LOAD} = 0$	0		2.5	4	mA
I <sub>HBS</sub>	HB to $V_{\mbox{\scriptsize SS}}$ quiescent current		$V_{HS} = V_{HB} = 110 \text{ V}$			0.000 5	1	μA
I <sub>HBSO</sub>	HB to $V_{SS}$ operating current		$f = 500 \text{ kHz}, C_{LOAD} = 0$	0		0.1		mA
Input								
V <sub>HIT</sub>	Input rising threshold	UCC27200				5.8	8	V
$V_{LIT}$	Input falling threshold	UCC27200			3	5.4		V
V <sub>IHYS</sub>	Input voltage hysteresis	UCC27200				0.4		V
V <sub>HIT</sub>	Input voltage threshold	UCC27201				1.7	2.5	V
V <sub>LIT</sub>	Input voltage threshold	UCC27201			0.8	1.6		V
V <sub>IHYS</sub>	Input voltage hysteresis	UCC27201				100		mV
R <sub>IN</sub>	Input pulldown resistance				100	200	350	kΩ
Underv	oltage Lockout (UVLO) Protection							
	V <sub>DD</sub> rising threshold				6.2	7.1	7.8	V
	V <sub>DD</sub> threshold hysteresis					0.5		V
	VHB rising threshold			5.8	6.7	7.2	V	
	VHB threshold hysteresis					0.4		V
Bootstr	ap Diode							
V <sub>F</sub>	Low-current forward voltage		$I_{VDD} - HB = 100 \ \mu A$			0.65	0.85	v
V <sub>FI</sub>	High-current forward voltage		$I_{VDD} - HB = 100 \text{ mA}$			0.85	1.1	v
R <sub>D</sub>	Dynamic resistance, $\Delta VF/\Delta I$		$I_{VDD} - HB = 100 \text{ mA} \text{ and } 80 \text{ mA}$			0.6	1.0	Ω
LO Gate	e Driver							
V <sub>LOL</sub>	Low level output voltage		I <sub>LO</sub> = 100 mA			0.18	0.4	V
V <sub>LOH</sub>	High level output voltage		I <sub>LO</sub> = -100 mA,	$T_J = -40^{\circ}C$ to $125^{\circ}C$		0.25	0.4	v
LOH	high level output voltage		$V_{LOH} = V_{DD} - V_{LO}$	$T_J = -40^{\circ}C$ to $140^{\circ}C$		0.25	0.42	v
	Peak pullup current		$V_{LO} = 0 V$			3		Α
	Peak pulldown current		$V_{LO} = 12 V$			3		Α
HO Gate	e Driver							
V <sub>HOL</sub>	Low-level output voltage		I <sub>HO</sub> = 100 mA			0.18	0.4	V
Vue	V <sub>HOH</sub> High-level output voltage		I <sub>HO</sub> = -100 mA,	$T_{J} = -40^{\circ}C$ to 125°C $T_{J} = -40^{\circ}C$ to 140°C		0.25	0.4	v
V <sub>HOH</sub>	i igni ievel output voltage		$V_{HOH} = V_{HB} - V_{HO},$		0.25	0.42	v	
	Peak pullup current		V <sub>HO</sub> = 0 V			3		А
	Peak pulldown current		V <sub>HO</sub> = 12 V			3		Α



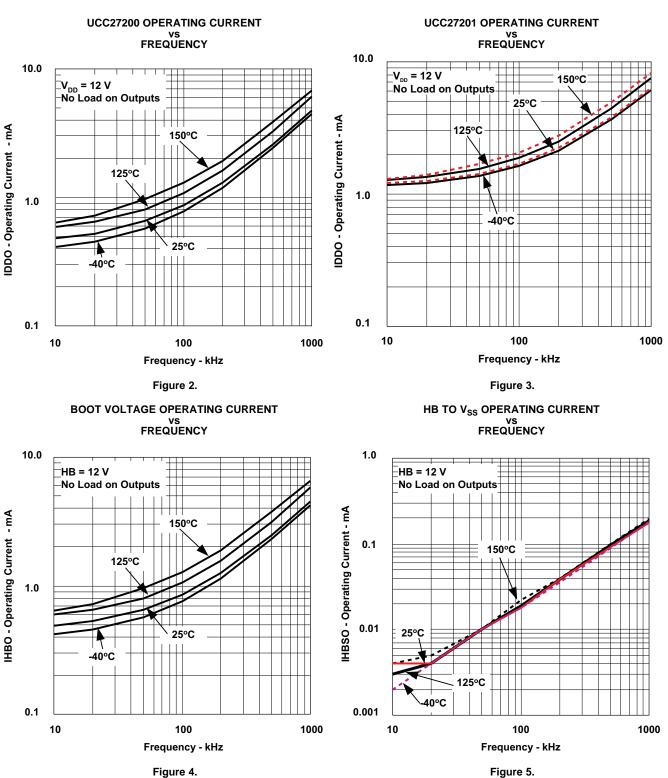
## **ELECTRICAL CHARACTERISTICS (continued)**

over operating free-air temperature range,  $V_{DD} = V_{HB} = 12$  V,  $V_{HS} = V_{SS} = 0$  V, No load on LO or HO,  $T_A = T_J = -40^{\circ}$ C to 140°C (unless otherwise noted)

	PARAMETER	TE	TEST CONDITIONS			MAX	UNIT
Propaga	ation Delays	<b>I</b>		1			
<b>-</b>	\/_folling_to \/_folling	0	$T_{J} = -40^{\circ}C$ to 125°C		20	45	ns
T <sub>DLFF</sub>	$V_{LI}$ falling to $V_{LO}$ falling	$C_{LOAD} = 0$	$T_{J} = -40^{\circ}C$ to 140°C		20	50	ns
<b>-</b>	\/ folling to \/ folling	0 0	$T_J = -40^{\circ}C$ to $125^{\circ}C$		20	45	ns
T <sub>DHFF</sub>	$V_{HI}$ falling to $V_{HO}$ falling	$C_{LOAD} = 0$	$T_{\rm J} = -40^{\circ}{\rm C}$ to $140^{\circ}{\rm C}$		20	50	ns
<b>-</b>	V riging to V riging	0 0	$T_J = -40^{\circ}C$ to $125^{\circ}C$		20	45	ns
T <sub>DLRR</sub> V <sub>LI</sub> rising to V <sub>LO</sub> rising		$C_{LOAD} = 0$	$T_{J} = -40^{\circ}C$ to $140^{\circ}C$		20	50	ns
	V ricing to V ricing	0 0	$T_{J} = -40^{\circ}C$ to 125°C		20	45	ns
T <sub>DHRR</sub>	V <sub>HI</sub> rising to V <sub>HO</sub> rising	$C_{LOAD} = 0$	$T_{J} = -40^{\circ}C$ to $140^{\circ}C$		20	50	ns
Delay M	latching						
T <sub>MON</sub>	LI ON, HI OFF				1	7	ns
T <sub>MOFF</sub>	LI OFF, HI ON				1	7	ns
Output I	Rise and Fall Time						
t <sub>R</sub>	LO, HO	C <sub>LOAD</sub> = 1000 pF			8		ns
t <sub>F</sub>	LO, HO	C <sub>LOAD</sub> = 1000 pF			7		ns
t <sub>R</sub>	LO, HO (3 V to 9 V)	$C_{LOAD} = 0.1 \ \mu F$		0.35	0.6	μs	
t <sub>F</sub>	LO, HO (3 V to 9 V)	$C_{LOAD} = 0.1 \ \mu F$			0.3	0.6	μs
Miscella	ineous	· ·					
	Minimum input pulse width that changes the output					50	ns
	Bootstrap diode turn-off time	= 0.5 A <sup>(1)(2)</sup>		20		ns	

(1) Typical values for  $T_A = 25^{\circ}C$ (2)  $I_F$ : Forward current applied to bootstrap diode.  $I_{REV}$ : Reverse current applied to bootstrap diode.

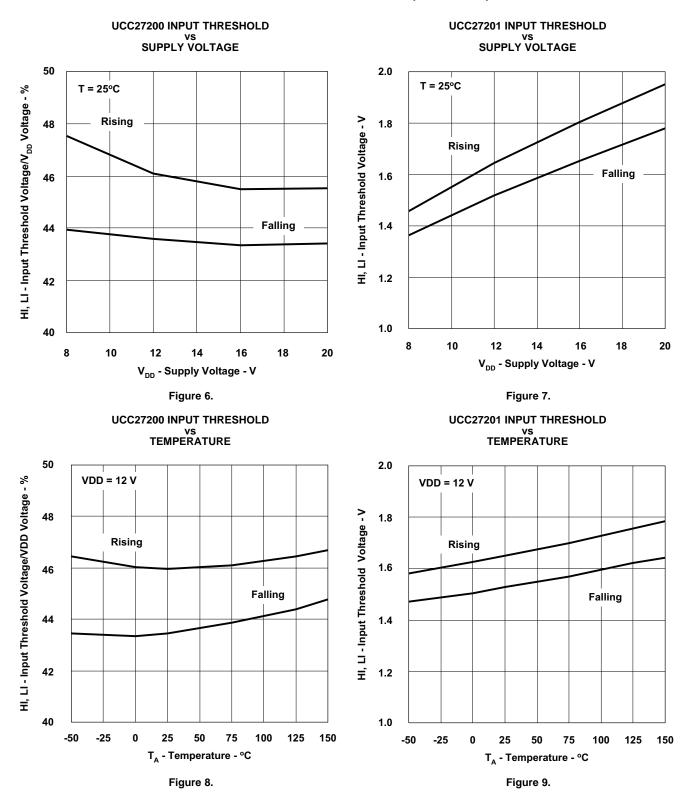




## **TYPICAL CHARACTERISTICS**

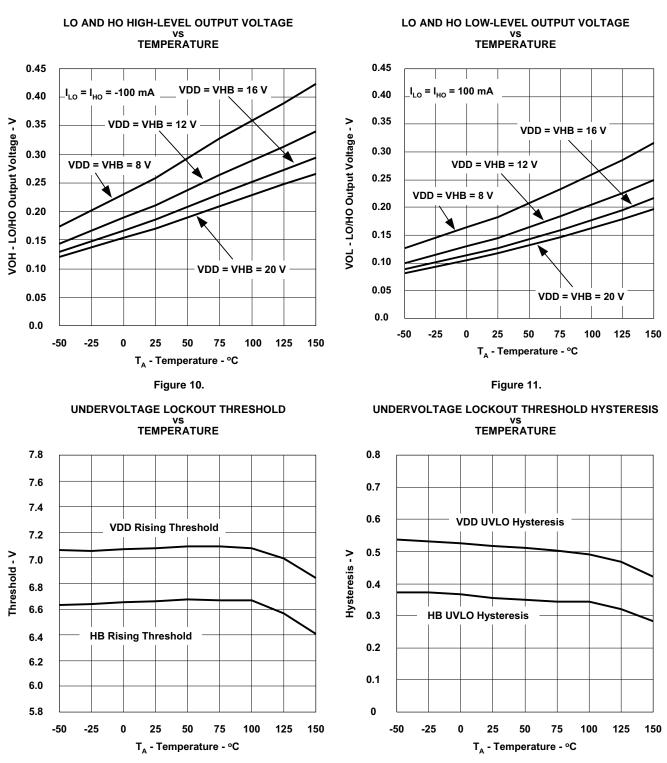


## **TYPICAL CHARACTERISTICS (continued)**



TEXAS INSTRUMENTS

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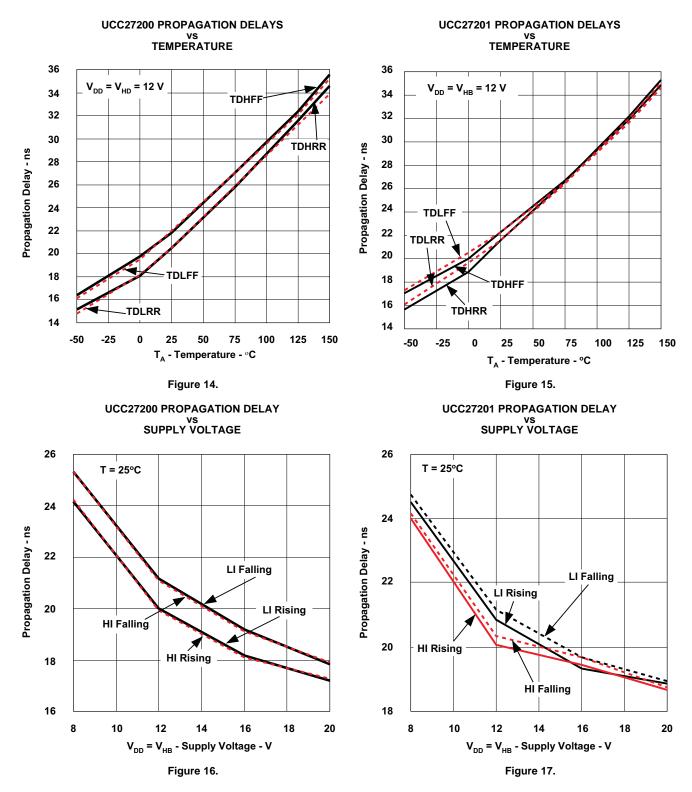
## **TYPICAL CHARACTERISTICS (continued)**

Figure 13.

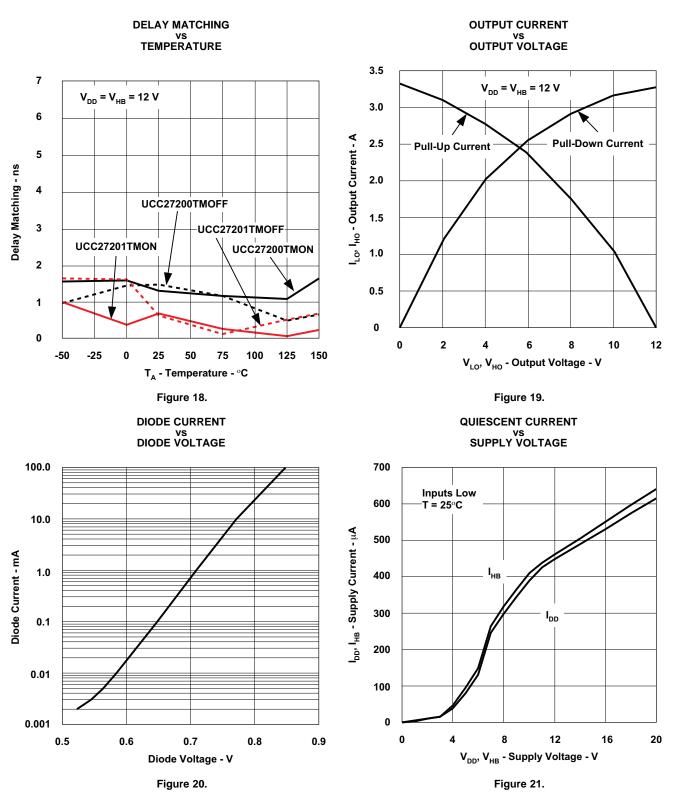
Figure 12.







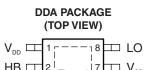




## **TYPICAL CHARACTERISTICS (continued)**



### **DEVICE INFORMATION**



 $HB \square 2 | HB \square 4 | H$ 

A. The  $V_{\text{SS}}$  pin and the exposed thermal die pad are internally connected.

#### **TERMINAL FUNCTIONS**

TERMINAL		- I/O	DECODIDION
NAME	NO.	1/0	DESCRIPTION
V <sub>DD</sub>	1	I	Positive supply to the lower gate driver. Decouple this pin to V_{SS} (GND). Typical decoupling capacitor range is 0.22 $\mu F$ to 1.0 $\mu F.$
НВ	2	I	High-side bootstrap supply. The bootstrap diode is on-chip, but the external bootstrap capacitor is required. Connect positive side of the bootstrap capacitor to this pin. Typical range of HB bypass capacitor is 0.022 $\mu$ F to 0.1 $\mu$ F, however, the value is dependant on the gate charge of the high-side MOSFET.
НО	3	0	High-side output. Connect to the gate of the high-side power MOSFET.
HS	4	I	High-side source connection. Connect to source of high-side power MOSFET. Connect negative side of bootstrap capacitor to this pin.
н	5	I	High-side input
LI	6	I	Low-side input
V <sub>SS</sub>	7	0	Negative supply terminal for the device which is generally grounded
LO	8	0	Low-side output. Connect to the gate of the low-side power MOSFET.
PowerPAD	PAD		Electrically referenced to $V_{\text{SS}}$ (GND). Connect to a large thermal mass trace or GND plane to dramatically improve thermal performance.

TEXAS INSTRUMENTS

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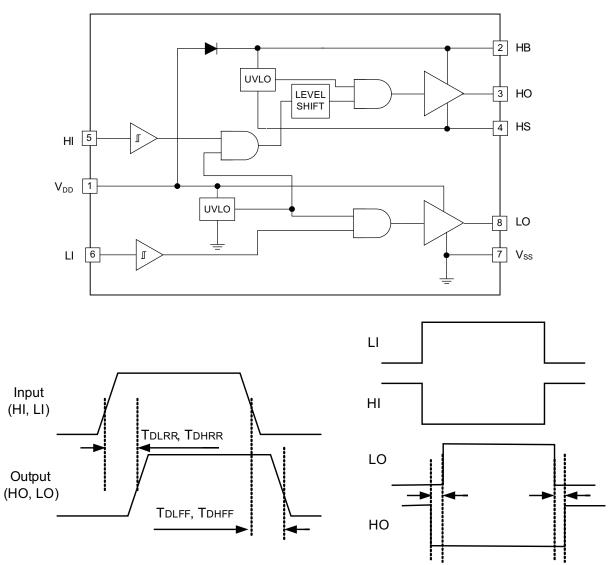


Figure 22. Timing Diagrams

TMOFF

TMON



## **APPLICATION INFORMATION**

### **Functional Description**

The UCC27200 and UCC27201 are high-side/low-side drivers. The high side and low side each have independent inputs, which allow maximum flexibility of input control signals in the application. The boot diode for the high-side driver bias supply is internal to the UCC27200 and UCC27201. The UCC27200 is the CMOS-compatible input version, and the UCC27201 is the TTL- or logic-compatible version. The high-side driver is referenced to the switch node (HS), which is typically the source pin of the high side MOSFET and drain pin of the low-side MOSFET. The low-side driver is referenced to V<sub>SS</sub>, which is typically ground. The functions contained are the input stages, UVLO protection, level shift, boot diode, and output driver stages.

#### NOTE:

The term UCC2720x applies to both the UCC27200 and UCC27201.

#### Input Stages

The input stages provide the interface to the PWM output signals. The input impedance of the UCC27200 is 200 k $\Omega$  nominal and input capacitance is approximately 2 pF. The 200 k $\Omega$  is a pulldown resistance to Vss (ground). The CMOS compatible input of the UCC27200 provides a rising threshold of 48% of V<sub>DD</sub> and falling threshold of 45% of V<sub>DD</sub>. The inputs of the UCC27200 are intended to be driven from 0 to V<sub>DD</sub> levels.

The input stages of the UCC27201 incorporate an open drain configuration to provide the lower input thresholds. The input impedance is 200 k $\Omega$  nominal and input capacitance is approximately 4 pF. The 200 k $\Omega$  is a pulldown resistance to V<sub>SS</sub> (ground). The logic level compatible input provides a rising threshold of 1.7 V and a falling threshold of 1.6 V.

#### Undervoltage Lockout (UVLO)

The bias supplies for the high-side and low-side drivers have UVLO protection.  $V_{DD}$  as well as  $V_{HB}$  to  $V_{HS}$  differential voltages are monitored. The  $V_{DD}$  UVLO disables both drivers when  $V_{DD}$  is below the specified threshold. The rising  $V_{DD}$  threshold is 7.1 V with 0.5-V hysteresis. The  $V_{HB}$  UVLO disables only the high-side driver when the  $V_{HB}$  to  $V_{HS}$  differential voltage is below the specified threshold. The  $V_{HB}$  UVLO rising threshold is 6.7 V with 0.4-V hysteresis.

#### Level Shift

The level-shift circuit is the interface from the high-side input to the high-side driver stage, which is referenced to the switch node (HS). The level shift allows control of the HO output referenced to the HS pin and provides excellent delay matching with the low-side driver.

#### Boot Diode

The boot diode necessary to generate the high-side bias is included in the UCC2720x family of drivers. The diode anode is connected to  $V_{DD}$  and cathode connected to VHB. With the VHB capacitor connected to HB and the HS pins, the  $V_{HB}$  capacitor charge is refreshed every switching cycle when HS transitions to ground. The boot diode provides fast recovery times, low diode resistance, and a voltage rating margin that allow for efficient and reliable operation.

#### **Output Stages**

The output stages are the interface to the power MOSFETs in the power train. High slew rate, low resistance and high peak current capability of both output drivers allow for efficient switching of the power MOSFETs. The low-side output stage is referenced from  $V_{DD}$  to  $V_{SS}$  and the high-side is referenced from  $V_{HB}$  to  $V_{HS}$ .

Switching the MOSFETs

SLUS822A-JUNE 2008-REVISED NOVEMBER 2008

UCC27200-Q1

UCC27201-Q1

**Design Tips** 

Achieving optimum drive performance at high frequency efficiently requires special attention to layout and minimizing parasitic inductances. Care must be taken at the driver die and package level as well as the PCB layout to reduce parasitic inductances as much as possible. Figure 23 shows the main parasitic inductance elements and current flow paths during the turn on and turn off of the MOSFET by charging and discharging its CGS capacitance.

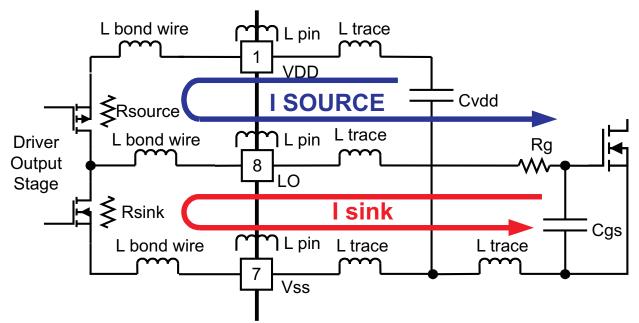
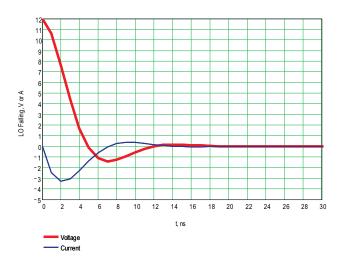


Figure 23. MOSFET Drive Paths and Circuit Parasitics

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The  $I_{SOURCE}$  current charges the  $C_{GS}$  gate capacitor and the  $I_{SINK}$  current discharges it. The rise and fall time of the voltage across the gate to source defines how quickly the MOSFET can be switched. Based on actual measurements, the analytical curves in Figure 24 and Figure 25 indicate the output voltage and current of the drivers during the discharge of the load capacitor. Figure 24 shows voltage and current as a function of time. Figure 25 indicates the relationship of voltage and current during fast switching. These figures demonstrate the actual switching process and limitations due to parasitic inductances.



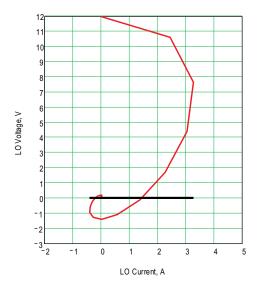


Figure 24. Turn-Off Voltage and Current vs Time

Figure 25. Turn-Off Voltage and Current Switching

### UCC27200-Q1 UCC27201-Q1 SLUS822A-JUNE 2008-REVISED NOVEMBER 2008



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Turning off the MOSFET must be achieved as fast as possible to minimize switching losses. For this reason, the UCC2720x drivers are designed for high peak currents and low output resistance. The sink capability is specified as 0.18 V at 100-mA dc current, implying  $1.8 \cdot \Omega R_{DS(on)}$ . With 12-V drive voltage, no parasitic inductance, and a linear resistance, one would expect initial sink current amplitude of 6.7 A for both high-side and low-side drivers. Assuming a pure R-C discharge circuit of the gate capacitor, one would expect the voltage and current waveforms to be exponential. Due to the parasitic inductances and nonlinear resistance of the driver MOSFETs, the actual waveforms have some ringing, and the peak sink current of the drivers is approximately 3.3 A, as shown in Figure 19. The overall parasitic inductance of the drive circuit is estimated at 4 nH.

Actual measured waveforms are shown in Figure 26 and Figure 27. As shown, the typical rise time of 8 ns and fall time of 7 ns is conservatively rated.

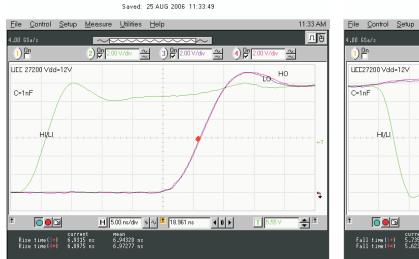


Figure 26.  $V_{\text{LO}}$  and  $V_{\text{HO}}$  Rise Time, 1-nF Load, 5 ns/Div



Figure 27.  $V_{LO}$  and  $V_{HO}$  Fall Time, 1-nF Load, 5-ns/Div



#### **Dynamic Switching of the MOSFETs**

The true behavior of MOSFETS presents a dynamic capacitive load primarily at the gate to source threshold voltage. Using the turn-off case as the example, when the gate to source threshold voltage is reached, the drain voltage starts rising, and the drain-to-gate parasitic capacitance couples charge into the gate, resulting in the turn-off plateau. The relatively low threshold voltages of many MOSFETS and the increased charge that must be removed (Miller charge) makes good driver performance necessary for efficient switching. An open-loop half-bridge power converter was utilized to evaluate performance in actual applications. The schematic of the half-bridge converter is shown in Figure 30. The turn-off waveforms of the UCC27200 driving two MOSFETs in parallel are shown in Figure 28 and Figure 29.

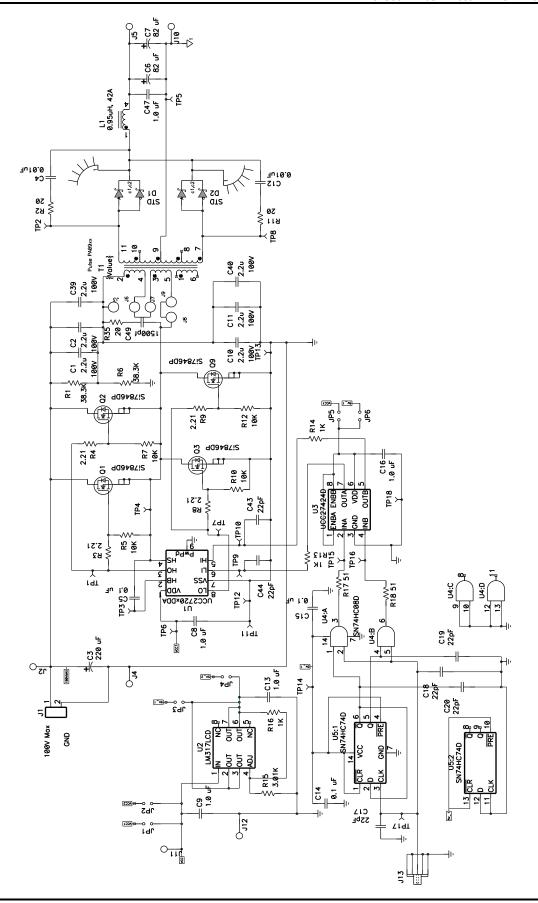


Figure 28. V<sub>LO</sub> Fall Time in Half-Bridge Converter

Figure 29. V<sub>HO</sub> Fall Time in Half-Bridge Converter









#### Figure 30. Open-Loop Half-Bridge Converter



#### **Delay Matching and Narrow Pulse Widths**

The total delays encountered in the PWM, driver, and power stage must be considered for a number of reasons, primarily for the delay in current limit response. Also to be considered are differences in delays between the drivers which can lead to various concerns depending on the topology. The sync-buck topology switching requires careful selection of dead time between the high- and low-side switches to avoid cross conduction and excessive body diode conduction. Bridge topologies can be affected by a resulting volt-sec imbalance on the transformer, if there is imbalance in the high- and low-side pulse widths in a steady-state condition.

Narrow pulse width performance is an important consideration when transient and short circuit conditions are encountered. Although there may be relatively long steady state PWM output-driver-MOSFET signals, very narrow pulses may be encountered in soft start, large load transients, and short-circuit conditions.

The UCC2720x driver family offers excellent performance in high- and low-side driver delay matching and narrow pulse width performance. The delay matching waveforms are shown in Figure 31 and Figure 32. The UCC2720x driver narrow pulse performance is shown in Figure 33 and Figure 34.



Figure 31.  $V_{LO}$  and  $V_{HO}$  Rising Edge Delay Matching





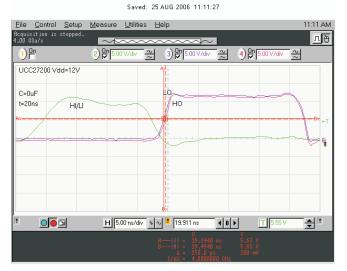


Figure 33. 20-ns Input Pulse Delay Matching





UCC27200-Q1 UCC27201-Q1 SLUS822A-JUNE 2008-REVISED NOVEMBER 2008



#### **Boot-Diode Performance**

The UCC2720x family of drivers internally incorporates the bootstrap diode necessary to generate the high-side bias. The characteristics of this diode are important to achieve efficient reliable operation. The dc characteristics to consider are V<sub>F</sub> and dynamic resistance. A low V<sub>F</sub> and high dynamic resistance results in a high forward voltage during charging of the bootstrap capacitor. The UCC2720x has a boot diode rated at 0.65-V V<sub>F</sub> and dynamic resistance of 0.6  $\Omega$  for reliable charge transfer to the bootstrap capacitor. The dynamic characteristics to consider are diode recovery time and stored charge. Diode recovery times that are specified with no conditions can be misleading. Diode recovery times at no forward current (I<sub>F</sub>) can be noticeably less than with forward current applied. The UCC2720x boot diode recovery is specified at 20 ns at I<sub>F</sub> = 20 mA, I<sub>REV</sub> = 0.5 A. At 0-mA I<sub>F</sub>, the reverse recovery time is 15 ns.

Another less obvious consideration is how the stored charge of the diode is affected by applied voltage. On every switching transition when the HS node transitions from low to high, charge is removed from the boot capacitor to charge the capacitance of the reverse-biased diode. This is a portion of the driver power losses and it reduces the voltage on the HB capacitor. At higher applied voltages, the stored charge of the UCC2720x PN diode is often less than a comparable Schottky diode.

#### Layout Recommendations

To improve the switching characteristics and efficiency of a design, the following layout rules should be followed.

- Locate the driver as close as possible to the MOSFETs.
- Locate the  $V_{DD}$  and  $V_{HB}$  (bootstrap) capacitors as close as possible to the driver.
- Pay close attention to the GND trace. Use the thermal pad of the DDA package as GND by connecting it to the V<sub>SS</sub> pin (GND). Note: The GND trace from the driver goes directly to the source of the MOSFET but should not be in the high current path of the MOSFET(S) drain or source current.
- Use similar rules for the HS node as for GND for the high side driver.
- Use wide traces for LO and HO closely following the associated GND or HS traces. Where possible, widths of 60 mil to 100 mil are preferred.
- Use two or more vias if the driver outputs or SW node need to be routed from one layer to another. For GND, the number of vias should be a consideration of the thermal pad requirements as well as parasitic inductance.
- Avoid L<sub>I</sub> and H<sub>I</sub> (driver input) going close to the HS node or any other high dV/dT traces that can induce significant noise into the relatively high-impedance leads.
- Keep in mind that a poor layout can cause a significant drop in efficiency versus a good PCB layout and can even lead to decreased reliability of the whole system.



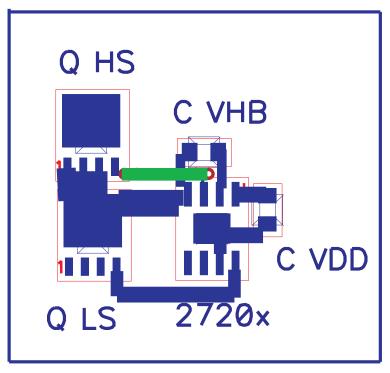


Figure 35. Example Component Placement

## **Additional References**

These references and links to additional information may be found at www.ti.com.

- 1. Additional layout guidelines for PCB land patterns may be found in application brief SLUA271.
- 2. Additional thermal performance guidelines may be found in application reports SLMA002 and SLMA004.



11-Apr-2013

## **PACKAGING INFORMATION**

Orderable Device	Status	Package Type	•	Pins	•	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Top-Side Markings	Samples
	(1)		Drawing		Qty	(2)		(3)		(4)	
UCC27200QDDARQ1	ACTIVE	SO PowerPAD	DDA	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-4-260C-72 HR	-40 to 125	27200Q	Samples
UCC27201QDDARQ1	ACTIVE	SO PowerPAD	DDA	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-4-260C-72 HR	-40 to 125	27201Q	Samples

<sup>(1)</sup> The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes. **Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between

the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

<sup>(3)</sup> MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

<sup>(4)</sup> Multiple Top-Side Markings will be inside parentheses. Only one Top-Side Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Top-Side Marking for that device.

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OTHER QUALIFIED VERSIONS OF UCC27200-Q1, UCC27201-Q1 :



## PACKAGE OPTION ADDENDUM

11-Apr-2013

• Catalog: UCC27200, UCC27201

NOTE: Qualified Version Definitions:

• Catalog - TI's standard catalog product

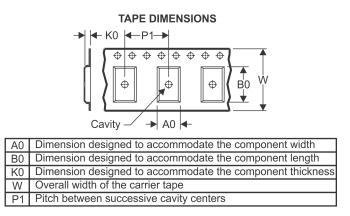
## PACKAGE MATERIALS INFORMATION

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## TAPE AND REEL INFORMATION





## QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal												
Device		Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
UCC27200QDDARQ1	SO Power PAD	DDA	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
UCC27201QDDARQ1	SO Power PAD	DDA	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1

TEXAS INSTRUMENTS

www.ti.com

## PACKAGE MATERIALS INFORMATION

23-Nov-2013



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
UCC27200QDDARQ1	SO PowerPAD	DDA	8	2500	367.0	367.0	35.0
UCC27201QDDARQ1	SO PowerPAD	DDA	8	2500	367.0	367.0	35.0

DDA (R-PDSO-G8)

PowerPAD ™ PLASTIC SMALL-OUTLINE



- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusion not to exceed 0,15.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>.
- E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions.
- F. This package complies to JEDEC MS-012 variation BA

PowerPAD is a trademark of Texas Instruments.



## DDA (R-PDSO-G8)

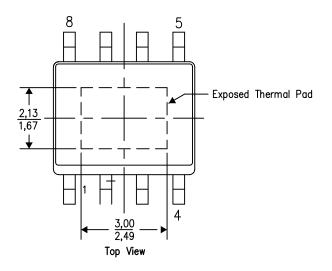
# PowerPAD<sup>™</sup> PLASTIC SMALL OUTLINE

## THERMAL INFORMATION

This PowerPAD<sup> $\mathbb{N}$ </sup> package incorporates an exposed thermal pad that is designed to be attached to a printed circuit board (PCB). The thermal pad must be soldered directly to the PCB. After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.



Exposed Thermal Pad Dimensions

4206322-5/L 05/12

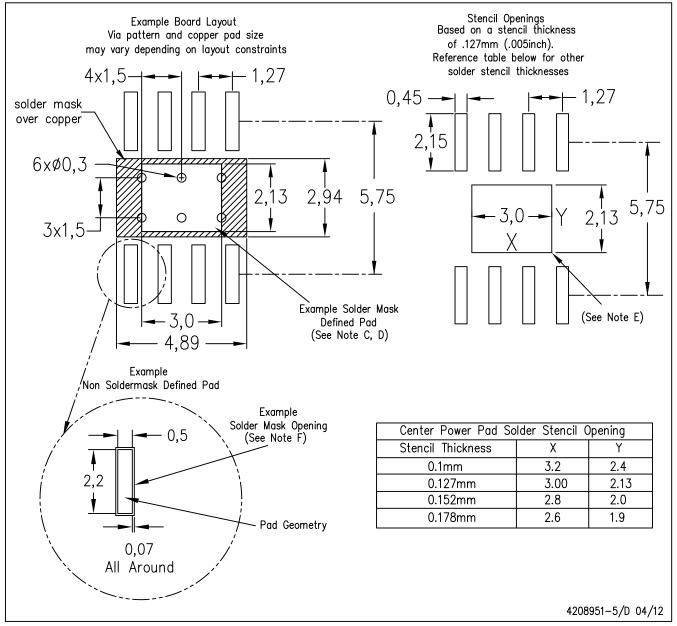
NOTE: A. All linear dimensions are in millimeters

PowerPAD is a trademark of Texas Instruments



DDA (R-PDSO-G8)

## PowerPAD<sup>™</sup> PLASTIC SMALL OUTLINE



NOTES:

- A. All linear dimensions are in millimeters.B. This drawing is subject to change without notice.
- C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002, SLMA004, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <http://www.ti.com>. Publication IPC-7351 is recommended for alternate designs.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.
- F. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads. PowerPAD is a trademark of Texas Instruments.



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