



## PRECISION ADJUSTABLE CURRENT-LIMITED POWER-DISTRIBUTION SWITCHES

Check for Samples: TPS2553-Q1

### **FEATURES**

- Qualified for Automotive Applications
- AEC-Q100 Qualified With the Following Results:
  - Device Temperature Grade 1: –40°C to 125°C Ambient Operating Temperature Range
  - Device HBM ESD Classification Level H2
  - Device CDM ESD Classification Level C3B
- Up to 1.5 A Maximum Load Current
- ±6% Current-Limit Accuracy at 1.7 A (typ)
- Meets USB Current-Limiting Requirements
- Backwards Compatible with TPS2550/51
- Adjustable current-limit, 75 mA-1300 mA (typ)
- Constant-Current (TPS2553-Q1)

- Fast Overcurrent Response 2-µs (typ)
- 85-mΩ High-Side MOSFET (DBV Package)
- Reverse Input-Output Voltage Protection
- Operating Range: 2.5 V to 6.5 V
- Built-in Soft-Start
- 15 kV ESD Protection per IEC 61000-4-2 (with External Capacitance)
- UL Listed File No. E169910 and NEMKO IEC60950-1-am1 ed2.0
- See the TI Switch Portfolio

## **APPLICATIONS**

- Automotive
- Power Distribution
- Current Limiting

## **DESCRIPTION**

The TPS2553-Q1 power-distribution switches are intended for applications where precision current-limiting is required or heavy capacitive loads and short circuits are encountered and provide up to 1.5 A of continuous load current. These devices offer a programmable current-limit threshold between 75 mA and 1.7 A (typ) via an external resistor. Current-limit accuracy as tight as ±6% can be achieved at the higher current-limit settings. The power-switch rise and fall times are controlled to minimize current surges during turn on/off.

TPS2553-Q1 devices limit the output current to a safe level by using a constant-current mode when the output load exceeds the current-limit threshold. An internal reverse- voltage comparator disables the power- switch when the output voltage is driven higher than the input to protect devices on the input side of the switch. The FAULT output asserts low during overcurrent and reverse-voltage conditions.

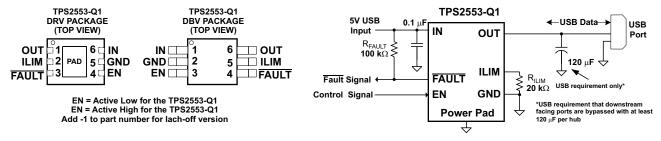


Figure 1. Typical Application as USB Power Switch

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.





This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

GENERAL SWITCH CATALOG												
33 mΩ, single  TPS201xA 0.2A-2A TPS202x 0.2A-2A TPS203x 0.2A-2A	80 mΩ, single  TPS2014 600 mA TPS2015 1 A TPS2041B 500 mA TPS2041B 500 mA TPS2049 100 mA TPS2049 100 mA TPS2065 250 mA TPS2065 1 A TPS2065 1 A TPS2065 1 A TPS2069 1.5 A	80 mΩ, dual  TPS2042B 500 mA TPS2052B 500 mA TPS2046B 250 mA TPS2066 1 A TPS2066 1 A TPS2066 1.5 A TPS2064 1.5 A	80 mΩ, dual  TPS2080 500 mA TPS2081 500 mA TPS2082 500 mA TPS2090 250 mA TPS2091 250 mA TPS2092 250 mA	80 mΩ, triple  TPS2043B 500 mA TPS2043B 500 mA TPS2047B 250 mA TPS2047A 250 mA TPS2063 1 A TPS2067 1 A		80 mΩ, quad  TPS2085 500 mA TPS2087 500 mA TPS2087 500 mA TPS2096 250 mA TPS2096 250 mA TPS2096 250 mA						

## ORDERING INFORMATION(1)

T <sub>A</sub> <sup>(2)</sup>	ENABLE	ORDERABLE PART NUMBER	TOP-SIDE MARKING	RECOMMENDED MAXIMUM CONTINUOUS LOAD CURRENT <sup>(2)</sup>	CURRENT-LIMIT PROTECTION	
-40°C to 125°C	Active high	TPS2553QDRVRQ1	TPS2553QDRVRQ1 Preview		Constant-Current	
-40 C to 125 C	Active high	TPS2553QDBVRQ1	PYEQ	1.5 A	Constant-Current	

- (1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.
- (2) Maximum ambient temperature is a function of device junction temperature and system level considerations, such as load current, power dissipation and board layout. See *dissipation rating table* and *recommended operating conditions* for specific information related to these devices.

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#### **ABSOLUTE MAXIMUM RATINGS**

over operating free-air temperature range unless otherwise noted(1) (2)

		VALUE	UNIT
	Voltage range on IN, OUT, EN or EN, ILIM, FAULT	–0.3 to 7	V
	Voltage range from IN to OUT	–7 to 7	V
Io	Continuous output current	Internally Limited	
	Continuous FAULT sink current	25	mA
	ILIM source current	1	mA
	Human Body Model Classification Level H2	2	kV
ESD Ratings	Charged Device Model ESD Classification Level C3B	750	V
ramigo	IEC system level (contact/air) <sup>(3)</sup>	8 / 15	kV
$T_{J}$	Maximum junction temperature	-40 to 150	°C
T <sub>stg</sub>	Storage temperature	-65 to 150	°C

<sup>(1)</sup> Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### THERMAL INFORMATION

	TUEDMAL METRIC(1)	TPS2553-Q1	TPS2553-Q1	
THERMAL METRIC <sup>(1)</sup>		DBV (6 PINS)	DRV (6 PINS)	UNIT
$\theta_{JA}$	Junction-to-ambient thermal resistance	182.6	72	
$\theta_{JCtop}$	Junction-to-case (top) thermal resistance	122.2	85.3	
$\theta_{JB}$	Junction-to-board thermal resistance	29.4	41.3	900
ΨЈТ	Junction-to-top characterization parameter	20.8	1.7	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	28.9	41.7	
$\theta_{\text{JCbot}}$	Junction-to-case (bottom) thermal resistance	n/a	11.1	

(1) For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, SPRA953.

Product Folder Links: TPS2553-Q1

<sup>(2)</sup> Voltages are referenced to GND unless otherwise noted.

<sup>(3)</sup> Surges per EN61000-4-2. 1999 applied to output terminals of EVM. These are passing test levels, not failure threshold.



### RECOMMENDED OPERATING CONDITIONS

				MIN	MAX	UNIT	
V <sub>IN</sub>	Input voltage, IN			2.5	6.5	V	
$V_{EN}$	Enable voltage			0	6.5	V	
V <sub>IH</sub>	High-level input voltage on EN or EN	High-level input voltage on EN or EN				V	
V <sub>IL</sub>	Low-level input voltage on EN or EN				0.66	V	
	Continuous autout auronat OUT	-40 °C ≤ T <sub>J</sub> ≤ 125 °C		0	1.2	۸	
I <sub>OUT</sub>	Continuous output current, OUT	-40 °C ≤ T <sub>J</sub> ≤ 105 °C		0	1.5	Α	
R <sub>ILIM</sub>	Current-limit threshold resistor range (	nominal 1%) from ILIM to GND		15	232	kΩ	
Io	Continuous FAULT sink current			0	10	mA	
	Input de-coupling capacitance, IN to GND					μF	
_	Operating virtual junction	I <sub>OUT</sub> ≤ 1.2 A		-40	125	°C	
IJ	Operating virtual junction temperature <sup>(1)</sup>	I <sub>OUT</sub> ≤ 1.5 A		-40	105	·C	

<sup>(1)</sup> See "Dissipation Rating Table" and "Power Dissipation and Junction Temperature" sections for details on how to calculate maximum junction temperature for specific applications and packages.

## **ELECTRICAL CHARACTERISTICS**

over recommended operating conditions,  $V_{EN} = 0 \text{ V}$ , or  $V_{EN} = V_{IN}$ ,  $R_{FAULT} = 10 \text{ k}\Omega$  (unless otherwise noted)

	PARAMETER		TEST	CONDITIONS(1)		MIN	TYP	MAX	UNIT
POWE	R SWITCH					•			
		DBV package, T <sub>A</sub> =	25°C				85	95	
		DBV package, -40°0	C ≤T <sub>A</sub> ≤125°	С				135	
r <sub>DS(on)</sub>	Static drain-source on-state resistance	DRV package, T <sub>A</sub> =	25°C				100	115	$m\Omega$
		DRV package, –40°C ≤T <sub>A</sub> ≤105°C						140	
		DRV package, -40°0	C ≤T <sub>A</sub> ≤125°	С				150	
	Disa time autout	V <sub>IN</sub> = 6.5 V					1.1	1.5	
t <sub>r</sub>	Rise time, output	V <sub>IN</sub> = 2.5 V	$C_L = 1 \mu F$	$R_L = 100 \Omega$			0.7	1	mo
	F. II.	V <sub>IN</sub> = 6.5 V	(see Figure	<del>2</del> )		0.2		0.5	ms
t <sub>f</sub>	Fall time, output	V <sub>IN</sub> = 2.5 V				0.2		0.5	
ENABI	LE INPUT EN OR EN								
	Enable pin turn on/off threshold							1.1	V
I <sub>EN</sub>	Input current	$V_{EN} = 0 \text{ V or } 6.5 \text{ V}, V_{\overline{EN}} = 0 \text{ V or } 6.5 \text{ V}$				-0.5		0.5	μA
t <sub>on</sub>	Turnon time	0 1 5 5 100						3	ms
t <sub>off</sub>	Turnoff time	$C_L = 1 \mu F, R_L = 100$	$C_L$ = 1 $\mu$ F, $R_L$ = 100 $\Omega$ , (see Figure 2)					3	ms
CURRI	ENT-LIMIT					*		-	
				$R_{ILIM} = 15 \text{ k}\Omega$	–40°C ≤T <sub>A</sub> ≤105°C	1610	1700	1800	
				D 0010	T <sub>A</sub> = 25°C	1215	1295	1375	
				$R_{ILIM} = 20 \text{ k}\Omega$	–40°C ≤T <sub>A</sub> ≤125°C	1200	1295	1375	1
Ios	Current-limit threshold (Maximum DC or load) and Short-circuit current, OUT cor		vered to	D 40.01.0	T <sub>A</sub> = 25°C	490	520	550	mA
	load) and onor oreal current, oor cor	incolor to GIVD		$R_{ILIM} = 49.9 \text{ k}\Omega$	–40°C ≤T <sub>A</sub> ≤125°C	475	520	565	
				$R_{ILIM} = 210 \text{ k}\Omega$	1	100	130	150	
				ILIM shorted to I	N	50	75	100	
t <sub>IOS</sub>	Response time to short circuit	V <sub>IN</sub> = 5 V (see Figure 3)					2		μs
REVER	RSE-VOLTAGE PROTECTION	-							
	Reverse-voltage comparator trip point $(V_{OUT} - V_{IN})$					95	135	190	mV
	Time from reverse-voltage condition to MOSFET turn off	V <sub>IN</sub> = 5 V	<sub>IN</sub> = 5 V				5	7	ms

<sup>(1)</sup> Pulse-testing techniques maintain junction temperature close to ambient temperature; thermal effects must be taken into account separately.

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# **ELECTRICAL CHARACTERISTICS (continued)**

over recommended operating conditions,  $V_{\overline{EN}} = 0$  V, or  $V_{EN} = V_{IN}$ ,  $R_{FAULT} = 10$  k $\Omega$  (unless otherwise noted)

	PARAMETER	TES	T CONDITIONS <sup>(1)</sup>	MIN	TYP	MAX	UNIT
SUPPL	Y CURRENT			-		· ·	
I <sub>IN_off</sub>	Supply current, low-level output	V <sub>IN</sub> = 6.5 V, No load on OUT, V	V <sub>EN</sub> = 6.5 V or V <sub>EN</sub> = 0 V		0.1	1	μA
	Complete company binds local code of	V CEV No look of OUT	$R_{ILIM} = 20 \text{ k}\Omega$		120	140	μΑ
I <sub>IN_on</sub>	Supply current, high-level output	V <sub>IN</sub> = 6.5 V, No load on OUT	$R_{ILIM} = 210 \text{ k}\Omega$		100	120	μΑ
I <sub>REV</sub>	Reverse leakage current	$V_{OUT} = 6.5 \text{ V}, V_{IN} = 0 \text{ V}$	T <sub>A</sub> = 25 °C		0.01	1	μA
UNDE	RVOLTAGE LOCKOUT						
UVLO	Low-level input voltage, IN	V <sub>IN</sub> rising		2.35	2.45	V	
	Hysteresis, IN	T <sub>A</sub> = 25 °C		25		mV	
FAULT	FLAG					,	
V <sub>OL</sub>	Output low voltage, FAULT	I <sub>/FAULT</sub> = 1 mA				180	mV
	Off-state leakage	V <sub>/FAULT</sub> = 6.5 V				1	μΑ
	FAULT deglitch	FAULT assertion or de-assertion	5	8	11	ms	
	FAULT degilleri	FAULT assertion or de-assertion	ULT assertion or de-assertion due to reverse-voltage condition			6	ms
THERM	MAL SHUTDOWN	,		•			
	Thermal shutdown threshold			155			°C
	Thermal shutdown threshold in current-limit			135			°C
	Hysteresis				10		°C

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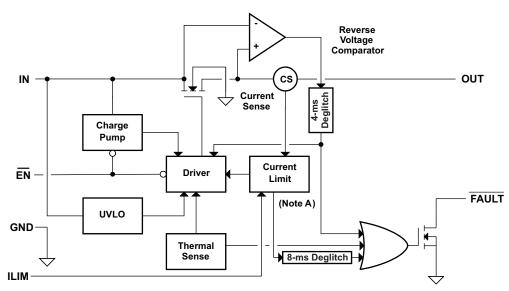
## **DEVICE INFORMATION**

## **Pin Functions**

	PIN			
NAME	TPS2553-Q1DBV NO.	TPS2553-Q1DRV NO.	I/O	DESCRIPTION
EN	_	_	I	Enable input, logic low turns on power switch
EN	3	4	I	Enable input, logic high turns on power switch
GND	2	5		Ground connection; connect externally to PowerPAD
IN	1	6	1	Input voltage; connect a 0.1 $\mu F$ or greater ceramic capacitor from IN to GND as close to the IC as possible.
FAULT	4	3	0	Active-low open-drain output, asserted during overcurrent, overtemperature, or reverse-voltage conditions.
OUT	6	1	0	Power-switch output
ILIM	5	2	0	External resistor used to set current-limit threshold; recommended 15 k $\Omega$ $\leq$ R <sub>ILIM</sub> $\leq$ 232 k $\Omega$ .
PowerPAD™	_	PAD		Internally connected to GND; used to heat-sink the part to the circuit board traces. Connect PowerPAD to GND pin externally.

Add -1 for Latch-Off version

## **FUNCTIONAL BLOCK DIAGRAM**



Note A: TPS255x parts enter constant current mode during current limit condition; TPS255x-1 parts latch off

## PARAMETER MEASUREMENT INFORMATION

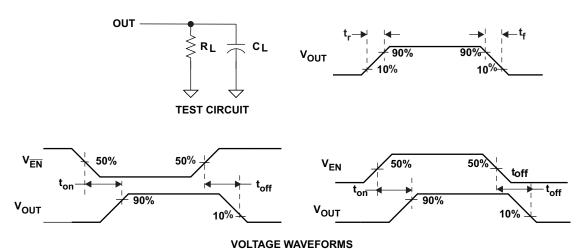


Figure 2. Test Circuit and Voltage Waveforms

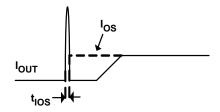


Figure 3. Response Time to Short Circuit Waveform

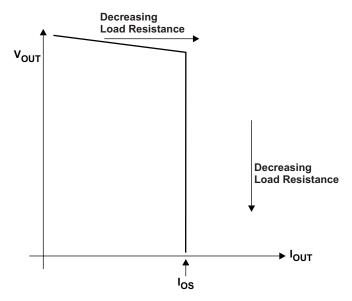


Figure 4. Output Voltage vs. Current-Limit Threshold



#### TYPICAL CHARACTERISTICS

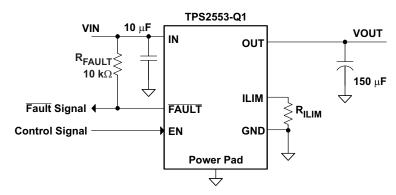


Figure 5. Typical Characteristics Reference Schematic

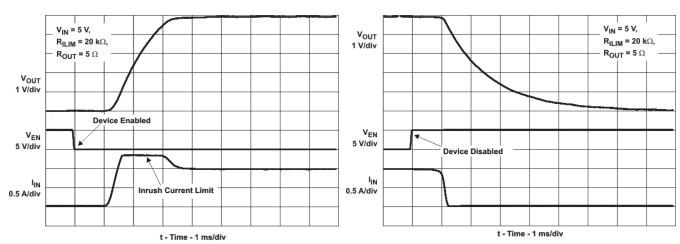
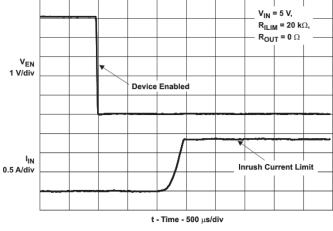


Figure 6. Turnon Delay and Rise Time

Figure 7. Turnoff Delay and Fall Time





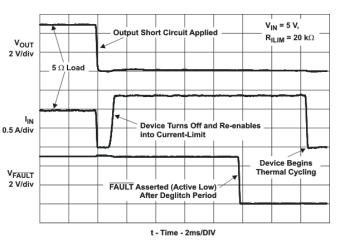


Figure 9. Full-Load to Short-Circuit Transient Response

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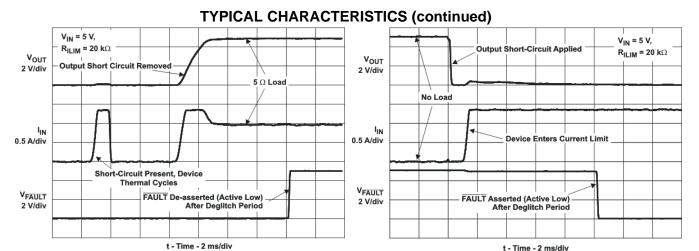


Figure 10. Short-Circuit to Full-Load Recovery Response

Figure 11. No-Load to Short-Circuit Transient Response

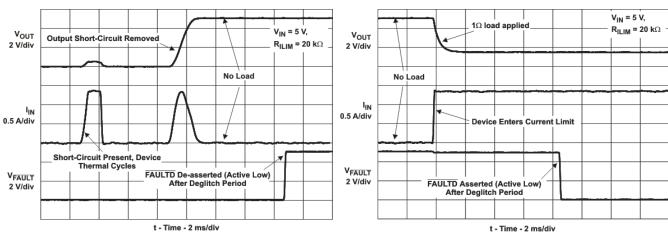


Figure 12. Short-Circuit to No-Load Recovery Response

Figure 13. No Load to 1Ω Transient Response

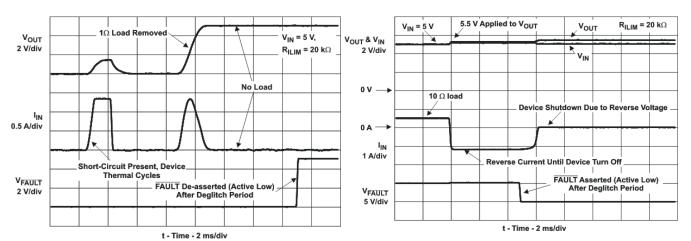


Figure 14.  $1\Omega$  to No Load Transient Response

Figure 15. Reverse-Voltage Protection Response







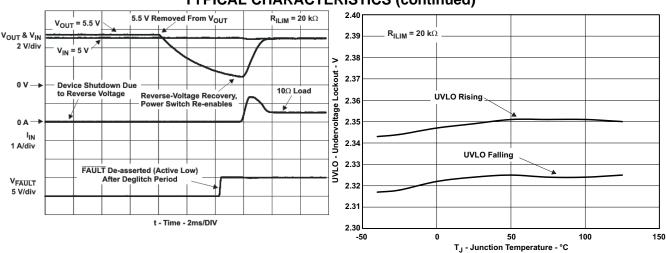


Figure 16. Reverse-Voltage Protection Recovery

Figure 17. UVLO - Undervoltage Lockout - V

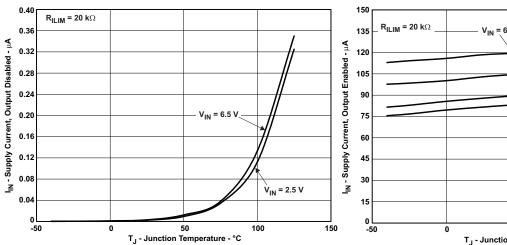


Figure 18.  $I_{IN}$  – Supply Current, Output Disabled –  $\mu A$ 

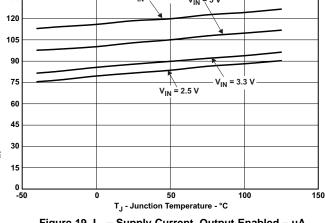
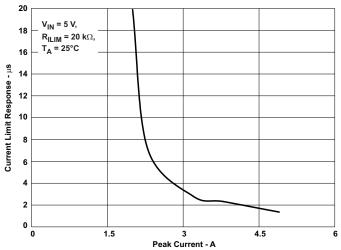


Figure 19.  $I_{IN}$  – Supply Current, Output Enabled –  $\mu A$ 





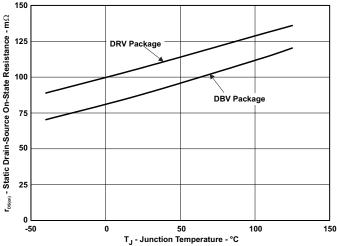


Figure 21. MOSFET  $r_{DS(on)}$  Vs. Junction Temperature

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100

200

300

400

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#### **TYPICAL CHARACTERISTICS (continued)** 1400 1300 140 130 1200 DS - Static Drain-Source Current - m4 1000 800 700 600 400 300 300 - Static Drain-Source Current - mA 120 T<sub>A</sub> = -40°C $T_A = -40$ °C T<sub>A</sub> = 25°C 110 T<sub>A</sub> = 25°C T<sub>A</sub> = 125°C 100 90 T<sub>A</sub> = 125°C 80 70 60 50 40 DS. 30 200 $V_{IN} = 6.5 V,$ V<sub>IN</sub> = 6.5 V, 20 $R_{ILIM} = 20 \text{ k}\Omega$ R<sub>ILIM</sub> = 200 kΩ 100

800

700

900

1000

10

100

200

V<sub>IN</sub> - V<sub>OUT</sub> - 100 mV/div Figure 22. Switch Current Vs. Drain-Source Voltage Across Switch

500

600

V<sub>IN</sub> - V<sub>OUT</sub> - 100 mV/div Figure 23. Switch Current Vs. Drain-Source Voltage Across Switch

500

600

800

900

1000



#### DETAILED DESCRIPTION

#### **OVERVIEW**

The TPS2553-Q1 is current-limited. Power-distribution switches using N-channel MOSFETs for applications where short circuits or heavy capacitive loads will be encountered and provide up to 1.5 A of continuous load current. These devices allow the user to program the current-limit threshold between 75 mA and 1.7 A (typ) via an external resistor. Additional device shutdown features include overtemperature protection and reverse-voltage protection. The device incorporates an internal charge pump and gate drive circuitry necessary to drive the Nchannel MOSFET. The charge pump supplies power to the driver circuit and provides the necessary voltage to pull the gate of the MOSFET above the source. The charge pump operates from input voltages as low as 2.5 V and requires little supply current. The driver controls the gate voltage of the power switch. The driver incorporates circuitry that controls the rise and fall times of the output voltage to limit large current and voltage surges and provides built-in soft-start functionality. The TPS2553-Q1 enters constant-current mode when the load exceeds the current-limit threshold.

#### **OVERCURRENT CONDITIONS**

The TPS2553-Q1 responds to overcurrent conditions by limiting the output current to the I<sub>OS</sub> levels shown in Figure 24. When an overcurrent condition is detected, the device maintains a constant output current and reduces the output voltage accordingly. Two possible overload conditions can occur.

The first condition is when a short circuit or partial short circuit is present when the device is powered-up or enabled. The output voltage is held near zero potential with respect to ground and the TPS2553-Q1 ramps the output current to IOS. The TPS2553-Q1 device will limit the current to IOS until the overload condition is removed or the device begins to thermal cycle. The device will remain off until power is cycled or the device enable is toggled.

The second condition is when a short circuit, partial short circuit, or transient overload occurs while the device is enabled and powered on. The device responds to the overcurrent condition within time t<sub>IOS</sub> (see Figure 3). The current-sense amplifier is overdriven during this time and momentarily disables the internal current-limit MOSFET. The current-sense amplifier recovers and limits the output current to I<sub>OS</sub>. Similar to the previous case, the TPS2553-Q1 will limit the current to I<sub>OS</sub> until the overload condition is removed or the device begins to thermal cycle.

The TPS2553-Q1 thermal cycles if an overload condition is present long enough to activate thermal limiting in any of the above cases. The device turns off when the junction temperature exceeds 135°C (typ) while in current-limit. The device remains off until the junction temperature cools 10°C (typ) and then restarts. The TPS2553-Q1 cycles on/off until the overload is removed (see Figure 10 and Figure 12).

## **REVERSE-VOLTAGE PROTECTION**

The reverse-voltage protection feature turns off the N-channel MOSFET whenever the output voltage exceeds the input voltage by 135 mV (typ) for 4-ms (typ). A reverse current of (V<sub>OUT</sub> - V<sub>IN</sub>)/r<sub>DS(on)</sub>) will be present when this occurs. This prevents damage to devices on the input side of the TPS2553-Q1 by preventing significant current from sinking into the input capacitance. The TPS2553-Q1 device allows the N-channel MOSFET to turn on once the output voltage goes below the input voltage for the same 4-ms deglitch time.

#### **FAULT RESPONSE**

The FAULT open-drain output is asserted (active low) during an overcurrent, overtemperature or reverse-voltage condition. The TPS2553-Q1 asserts the FAULT signal until the fault condition is removed and the device resumes normal operation. The TPS2553-Q1 is designed to eliminate false FAULT reporting by using an internal delay "deglitch" circuit for overcurrent (7.5-ms typ) and reverse-voltage (4-ms typ) conditions without the need for external circuitry. This ensures that FAULT is not accidentally asserted due to normal operation such as starting into a heavy capacitive load. The deglitch circuitry delays entering and leaving fault conditions. Overtemperature conditions are not deglitched and assert the FAULT signal immediately.

## **UNDERVOLTAGE LOCKOUT (UVLO)**

The undervoltage lockout (UVLO) circuit disables the power switch until the input voltage reaches the UVLO turnon threshold. Built-in hysteresis prevents unwanted on/off cycling due to input voltage drop from large current surges.

## **ENABLE (EN OR EN)**

The logic enable controls the power switch, bias for the charge pump, driver, and other circuits to reduce the supply current. The supply current is reduced to less than 1-µA when a logic high is present on EN or when a logic low is present on EN. A logic low input on EN or a logic high input on EN enables the driver, control circuits, and power switch. The enable input is compatible with both TTL and CMOS logic levels.

#### THERMAL SENSE

The TPS2553-Q1 has a self-protection feature using two independent thermal sensing circuits that monitor the operating temperature of the power switch. It disables the operation if the temperature exceeds recommended operating conditions. The TPS2553-Q1 device operates in constant-current mode during an overcurrent condition, which increases the voltage drop across the power-switch. The power dissipation in the package is proportional to the voltage drop across the power switch, which increases the junction temperature during an overcurrent condition. The first thermal sensor turns off the power switch when the die temperature exceeds 135°C (min) and the part is in current-limit. Hysteresis is built into the thermal sensor, and the switch turns on after the device has cooled approximately 10 °C.

The TPS2553-Q1 also has a second ambient thermal sensor. The ambient thermal sensor turns off the power-switch when the die temperature exceeds 155°C (min) regardless of whether the power switch is in current-limit and will turn on the power switch after the device has cooled approximately 10 °C. The TPS2553-Q1 continues to cycle off and on until the fault is removed.

The open-drain fault reporting output FAULT is asserted (active low) immediately during an overtemperature shutdown condition.

Product Folder Links: TPS2553-Q1

#### APPLICATION INFORMATION

#### INPUT AND OUTPUT CAPACITANCE

Input and output capacitance improves the performance of the device; the actual capacitance should be optimized for the particular application. For all applications, a  $0.1\mu F$  or greater ceramic bypass capacitor between IN and GND is recommended as close to the device as possible for local noise de-coupling. This precaution reduces ringing on the input due to power-supply transients. Additional input capacitance may be needed on the input to reduce voltage overshoot from exceeding the absolute maximum voltage of the device during heavy transient conditions. This is especially important during bench testing when long, inductive cables are used to connect the evaluation board to the bench power-supply.

Placing a high-value electrolytic capacitor on the output pin is recommended when large transient currents are expected on the output.

#### PROGRAMMING THE CURRENT-LIMIT THRESHOLD

The overcurrent threshold is user programmable via an external resistor. The TPS2553-Q1 uses an internal regulation loop to provide a regulated voltage on the ILIM pin. The current-limit threshold is proportional to the current sourced out of ILIM. The recommended 1% resistor range for  $R_{\text{ILIM}}$  is 15 k $\Omega \le R_{\text{ILIM}} \le 232$  k $\Omega$  to ensure stability of the internal regulation loop. Many applications require that the minimum current-limit is above a certain current level or that the maximum current-limit is below a certain current level, so it is important to consider the tolerance of the overcurrent threshold when selecting a value for  $R_{\text{ILIM}}$ . The following equations and Figure 24 can be used to calculate the resulting overcurrent threshold for a given external resistor value ( $R_{\text{ILIM}}$ ). Figure 24 includes current-limit tolerance due to variations caused by temperature and process. However, the equations do not account for tolerance due to external resistor variation, so it is important to account for this tolerance when selecting  $R_{\text{ILIM}}$ . The traces routing the  $R_{\text{ILIM}}$  resistor to the TPS2553-Q1 should be as short as possible to reduce parasitic effects on the current-limit accuracy.

R<sub>ILIM</sub> can be selected to provide a current-limit threshold that occurs 1) above a minimum load current or 2) below a maximum load current.

To design above a minimum current-limit threshold, find the intersection of  $R_{ILIM}$  and the maximum desired load current on the  $I_{OS(min)}$  curve and choose a value of  $R_{ILIM}$  below this value. Programming the current-limit above a minimum threshold is important to ensure start up into full load or heavy capacitive loads. The resulting maximum current-limit threshold is the intersection of the selected value of  $R_{ILIM}$  and the  $I_{OS(max)}$  curve.

To design below a maximum current-limit threshold, find the intersection of  $R_{ILIM}$  and the maximum desired load current on the  $I_{OS(max)}$  curve and choose a value of  $R_{ILIM}$  above this value. Programming the current-limit below a maximum threshold is important to avoid current-limiting upstream power supplies causing the input voltage bus to droop. The resulting minimum current-limit threshold is the intersection of the selected value of  $R_{ILIM}$  and the  $I_{OS(min)}$  curve.

Current-Limit Threshold Equations (I<sub>OS</sub>):

$$\begin{split} I_{OSmax}(mA) &= \frac{22980V}{R_{ILIM}^{0.94}k\Omega} \\ I_{OSnom}(mA) &= \frac{23950V}{R_{ILIM}^{0.977}k\Omega} \\ I_{OSmin}(mA) &= \frac{25230V}{R_{ILIM}^{1.016}k\Omega} \end{split}$$

(1)

where 15 k $\Omega \le R_{ILIM} \le 232 k\Omega$ .



While the maximum recommended value of RILIM is 232  $k\Omega$ , there is one additional configuration that allows for a lower current-limit threshold. The ILIM pin may be connected directly to IN to provide a 75 mA (typ) current-limit threshold. Additional low-ESR ceramic capacitance may be necessary from IN to GND in this configuration to prevent unwanted noise from coupling into the sensitive ILIM circuitry.

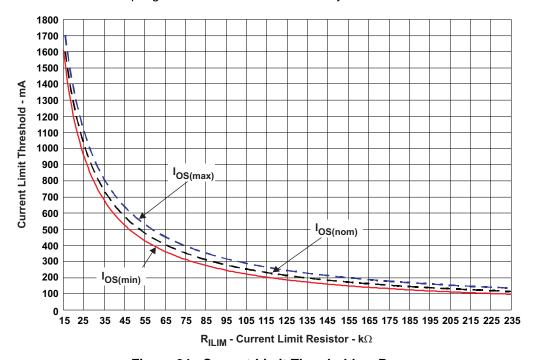


Figure 24. Current-Limit Threshold vs R<sub>ILIM</sub>

TEXAS INSTRUMENTS

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#### **APPLICATION 1: DESIGNING ABOVE A MINIMUM current-limit**

Some applications require that current-limiting cannot occur below a certain threshold. For this example, assume that 1 A must be delivered to the load so that the minimum desired current-limit threshold is 1000 mA. Use the  $I_{OS}$  equations and Figure 24 to select  $R_{ILIM}$ .

$$\begin{split} I_{OSmin}(mA) &= 1000mA \\ I_{OSmin}(mA) &= \frac{25230V}{R_{ILIM}^{1.016}k\Omega} \\ R_{ILIM}(k\Omega) &= \left(\frac{25230V}{I_{OSmin}mA}\right)^{\frac{1}{1.016}} \\ R_{ILIM}(k\Omega) &= 24k\Omega \end{split}$$

Select the closest 1% resistor less than the calculated value:  $R_{ILIM} = 23.7 \text{ k}\Omega$ . This sets the minimum current-limit threshold at 1 A . Use the  $I_{OS}$  equations, Figure 24, and the previously calculated value for  $R_{ILIM}$  to calculate the maximum resulting current-limit threshold.

$$\begin{split} R_{ILIM}(k\Omega) &= 23.7 k\Omega \\ I_{OSmax}(mA) &= \frac{22980 V}{R_{ILIM}^{0.94} k\Omega} \\ I_{OSmax}(mA) &= \frac{22980 V}{23.7^{0.94} k\Omega} \\ I_{OSmax}(mA) &= 1172.4 mA \end{split}$$

The resulting maximum current-limit threshold is 1172.4 mA with a 23.7 k $\Omega$  resistor.

### **APPLICATION 2: DESIGNING BELOW A MAXIMUM current-limit**

Some applications require that current-limiting must occur below a certain threshold. For this example, assume that the desired upper current-limit threshold must be below 500 mA to protect an up-stream power supply. Use the  $I_{OS}$  equations and Figure 24 to select  $R_{ILIM}$ .

$$\begin{split} I_{OSmax}(mA) &= 500mA \\ I_{OSmax}(mA) &= \frac{22980V}{R_{ILIM}^{0.94}k\Omega} \\ R_{ILIM}(k\Omega) &= \left(\frac{22980V}{I_{OSmax}mA}\right)^{\frac{1}{0.94}} \\ R_{ILIM}(k\Omega) &= 58.7k\Omega \end{split}$$

Select the closest 1% resistor greater than the calculated value:  $R_{ILIM}$  = 59 k $\Omega$ . This sets the maximum current-limit threshold at 500 mA . Use the I<sub>OS</sub> equations, Figure 24, and the previously calculated value for  $R_{ILIM}$  to calculate the minimum resulting current-limit threshold.

$$\begin{split} R_{ILIM}(k\Omega) &= 59k\Omega \\ I_{OSmin}(mA) &= \frac{25230V}{R_{ILIM}^{1.016}k\Omega} \\ I_{OSmin}(mA) &= \frac{25230V}{59^{1.016}k\Omega} \\ I_{OSmin}(mA) &= 400.6mA \end{split}$$
 (5)

The resulting minimum current-limit threshold is 400.6 mA with a 59 k $\Omega$  resistor.

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#### **ACCOUNTING FOR RESISTOR TOLERANCE**

The previous sections described the selection of  $R_{ILIM}$  given certain application requirements and the importance of understanding the current-limit threshold tolerance. The analysis focused only on the TPS2553-Q1 performance and assumed an exact resistor value. However, resistors sold in quantity are not exact and are bounded by an upper and lower tolerance centered around a nominal resistance. The additional  $R_{ILIM}$  resistance tolerance directly affects the current-limit threshold accuracy at a system level. The following table shows a process that accounts for worst-case resistor tolerance assuming 1% resistor values. Step one follows the selection process outlined in the application examples above. Step two determines the upper and lower resistance bounds of the selected resistor. Step three uses the upper and lower resistor bounds in the  $I_{OS}$  equations to calculate the threshold limits. It is important to use tighter tolerance resistors, e.g. 0.5% or 0.1%, when precision current-limiting is desired.

**Resistor Tolerance Actual Limits** Ideal Closest 1% **Desired Nominal** Resistor Resistor IOS MIN **IOS Nom IOS MAX** current-limit (mA) 1% low (kΩ) 1% high (kΩ)  $(k\Omega)$  $(k\Omega)$ (mA) (mA) (mA) SHORT ILIM to IN 75 50.0 75.0 100.0 120 101.3 120.0 142.1 226.1 226 223.7 228.3 200 134.0 133 131.7 134.3 173.7 201.5 233.9 300 88.5 88.7 87.8 89.6 262.1 299.4 342.3 400 65.9 66.5 65.8 67.2 351.2 396.7 448.7 500 52.5 52.3 51.8 448.3 501.6 562.4 52.8 43.5 43.2 42.8 544.3 604.6 673.1 600 43.6 37.4 37.0 37.8 630.2 696.0 770.8 700 37.2 800 32.4 32.4 32.1 32.7 729.1 8.008 882.1 900 28.7 28.7 28.4 29.0 824.7 901.5 988.7 1000 25.8 26.1 25.8 26.4 908.3 989.1 1081.0 23.2 23.0 23.4 1023.7 1109.7 1207.5 1100 23.4 1200 21.5 21.7 1106.0 1195.4 1297.1 21.4 21.3 19.6 19.4 1215.1 1308.5 1300 19.7 19.8 1414.9 1400 18.3 18.2 18.0 18.4 1310.1 1406.7 1517.0 1500 17.0 16.9 16.7 17.1 1412.5 1512.4 1626.4 1600 16.0 15.8 15.6 16.0 1512.5 1615.2 1732.7 1700 15.0 15.0 14.9 15.2 1594.5 1699.3 1819.4

Table 1. Common R<sub>ILIM</sub> Resistor Selections

## CONSTANT-CURRENT VS. LATCH-OFF OPERATION AND IMPACT ON OUTPUT VOLTAGE

During normal operation the constant-current device (TPS2553-Q1) has a load current that is less than the current-limit threshold and the device is not limiting current. During normal operation the N-channel MOSFET is fully enhanced, and  $V_{OUT} = V_{IN}$  - ( $I_{OUT} \times r_{DS(on)}$ ). The voltage drop across the MOSFET is relatively small compared to  $V_{IN}$ , and  $V_{OUT} \neq V_{IN}$ .

During the initial onset of an overcurrent event, the constant-current device (TPS2553-Q1) limits current to the programmed current-limit threshold set by  $R_{ILIM}$  by operating the N-channel MOSFET in the linear mode. During current-limit operation, the N-channel MOSFET is no longer fully-enhanced and the resistance of the device increases. This allows the device to effectively regulate the current to the current-limit threshold. The effect of increasing the resistance of the MOSFET is that the voltage drop across the device is no longer negligible ( $V_{IN} \neq V_{OUT}$ ), and  $V_{OUT}$  decreases. The amount that  $V_{OUT}$  decreases is proportional to the magnitude of the overload condition. The expected  $V_{OUT}$  can be calculated by  $I_{OS} \times R_{LOAD}$ , where  $I_{OS}$  is the current-limit threshold and  $R_{LOAD}$  is the magnitude of the overload condition. For example, if  $I_{OS}$  is programmed to 1 A and a 1  $\Omega$  overload condition is applied, the resulting  $V_{OUT}$  is 1  $V_{OUT}$ .

Product Folder Links: TPS2553-Q1

The constant-current device (TPS2553-Q1) operates during the initial onset of an overcurrent event, if the overcurrent event lasts longer than the internal delay "deglitch" circuit (7.5-ms typ). The constant-current device (TPS2553-Q1) asserts the FAULT flag after the deglitch period and continues to regulate the current to the current-limit threshold indefinitely. In practical circuits, the power dissipation in the package will increase the die temperature above the overtemperature shutdown threshold (135°C min), and the device will turn off until the die temperature decreases by the hysteresis of the thermal shutdown circuit (10°C typ). The device will turn on and continue to thermal cycle until the overload condition is removed. The constant-current devices resume normal operation once the overload condition is removed.

#### POWER DISSIPATION AND JUNCTION TEMPERATURE

The low on-resistance of the N-channel MOSFET allows small surface-mount packages to pass large currents. It is good design practice to estimate power dissipation and junction temperature. The below analysis gives an approximation for calculating junction temperature based on the power dissipation in the package. However, it is important to note that thermal analysis is strongly dependent on additional system level factors. Such factors include air flow, board layout, copper thickness and surface area, and proximity to other devices dissipating power. Good thermal design practice must include all system level factors in addition to individual component analysis.

Begin by determining the  $r_{DS(on)}$  of the N-channel MOSFET relative to the input voltage and operating temperature. As an initial estimate, use the highest operating ambient temperature of interest and read  $r_{DS(on)}$  from the typical characteristics graph. Using this value, the power dissipation can be calculated by:

$$P_D = r_{DS(on)} \times I_{OUT}^2$$

Where:

P<sub>D</sub> = Total power dissipation (W)

 $r_{DS(on)}$  = Power switch on-resistance ( $\Omega$ )

I<sub>OUT</sub> = Maximum current-limit threshold (A)

This step calculates the total power dissipation of the N-channel MOSFET.

Finally, calculate the junction temperature:

$$T_J = P_D \times \theta_{JA} + T_A$$

Where:

 $T_A$  = Ambient temperature (°C)

 $\theta_{JA}$  = Thermal resistance (°C/W)

P<sub>D</sub> = Total power dissipation (W)

Compare the calculated junction temperature with the initial estimate. If they are not within a few degrees, repeat the calculation using the "refined"  $r_{DS(on)}$  from the previous calculation as the new estimate. Two or three iterations are generally sufficient to achieve the desired result. The final junction temperature is highly dependent on thermal resistance  $\theta_{JA}$ , and thermal resistance is highly dependent on the individual package and board layout. The Thermal Information Table provides example thermal resistance for specific packages and board layouts.



## UNIVERSAL SERIAL BUS (USB) POWER-DISTRIBUTION REQUIREMENTS

One application for this device is for current-limiting in universal serial bus (USB) applications. The original USB interface was a 12-Mb/s or 1.5-Mb/s, multiplexed serial bus designed for low-to-medium bandwidth PC peripherals (e.g., keyboards, printers, scanners, and mice). As the demand for more bandwidth increased, the USB 2.0 standard was introduced increasing the maximum data rate to 480-Mb/s. The four-wire USB interface is conceived for dynamic attach-detach (hot plug-unplug) of peripherals. Two lines are provided for differential data, and two lines are provided for 5-V power distribution.

USB data is a 3.3-V level signal, but power is distributed at 5 V to allow for voltage drops in cases where power is distributed through more than one hub across long cables. Each function must provide its own regulated 3.3 V from the 5-V input or its own internal power supply. The USB specification classifies two different classes of devices depending on its maximum current draw. A device classified as low-power can draw up to 100 mA as defined by the standard. A device classified as high-power can draw up to 500 mA. It is important that the minimum current-limit threshold of the current-limiting power-switch exceed the maximum current-limit draw of the intended application. The latest USB standard should always be referenced when considering the current-limit threshold

The USB specification defines two types of devices as hubs and functions. A USB hub is a device that contains multiple ports for different USB devices to connect and can be self-powered (SPH) or bus-powered (BPH). A function is a USB device that is able to transmit or receive data or control information over the bus. A USB function can be embedded in a USB hub. A USB function can be one of three types included in the list below.

- Low-power, bus-powered function
- · High-power, bus-powered function
- Self-powered function

SPHs and BPHs distribute data and power to downstream functions. The TPS2553-Q1 has higher current capability than required for a single USB port allowing it to power multiple downstream ports.

Product Folder Links: TPS2553-Q1



#### **SELF-POWERED AND BUS-POWERED HUBS**

A SPH has a local power supply that powers embedded functions and downstream ports. This power supply must provide between 4.75 V to 5.25 V to downstream facing devices under full-load and no-load conditions. SPHs are required to have current-limit protection and must report overcurrent conditions to the USB controller. Typical SPHs are desktop PCs, monitors, printers, and stand-alone hubs.

A BPH obtains all power from an upstream port and often contains an embedded function. It must power up with less than 100 mA. The BPH usually has one embedded function, and power is always available to the controller of the hub. If the embedded function and hub require more than 100 mA on power up, the power to the embedded function may need to be kept off until enumeration is completed. This is accomplished by removing power or by shutting off the clock to the embedded function. Power switching the embedded function is not necessary if the aggregate power draw for the function and controller is less than 100 mA. The total current drawn by the bus-powered device is the sum of the current to the controller, the embedded function, and the downstream ports, and it is limited to 500 mA from an upstream port.

#### LOW-POWER BUS-POWERED AND HIGH-POWER BUS-POWERED FUNCTIONS

Both low-power and high-power bus-powered functions obtain all power from upstream ports. Low-power functions always draw less than 100 mA; high-power functions must draw less than 100 mA at power up and can draw up to 500 mA after enumeration. If the load of the function is more than the parallel combination of 44  $\Omega$  and 10  $\mu$ F at power up, the device must implement inrush current-limiting.

### **USB POWER-DISTRIBUTION REQUIREMENTS**

USB can be implemented in several ways regardless of the type of USB device being developed. Several power-distribution features must be implemented.

- · SPHs must:
  - current-limit downstream ports
  - Report overcurrent conditions
- BPHs must:
  - Enable/disable power to downstream ports
  - Power up at <100 mA</li>
  - Limit inrush current (<44 Ω and 10 μF)</li>
- Functions must:
  - Limit inrush currents
  - Power up at <100 mA</li>

The feature set of the TPS2553-Q1 meets each of these requirements. The integrated current-limiting and overcurrent reporting is required by self-powered hubs. The logic-level enable and controlled rise times meet the need of both input and output ports on bus-powered hubs and the input ports for bus-powered functions.

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#### **AUTO-RETRY FUNCTIONALITY**

Some applications require that an overcurrent condition disables the part momentarily during a fault condition and re-enables after a pre-set time. This auto-retry functionality can be implemented with an external resistor and capacitor. During a fault condition,  $\overline{FAULT}$  pulls low disabling the part. The part is disabled when EN is pulled low, and  $\overline{FAULT}$  goes high impedance allowing  $C_{RETRY}$  to begin charging. The part re-enables when the voltage on EN reaches the turnon threshold, and the auto-retry time is determined by the resistor/capacitor time constant. The part will continue to cycle in this manner until the fault condition is removed.

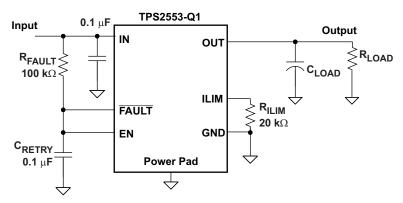


Figure 25. Auto-Retry Functionality

Some applications require auto-retry functionality and the ability to enable/disable with an external logic signal. The figure below shows how an external logic signal can drive EN through R<sub>FAULT</sub> and maintain auto-retry functionality. The resistor/capacitor time constant determines the auto-retry time-out period.

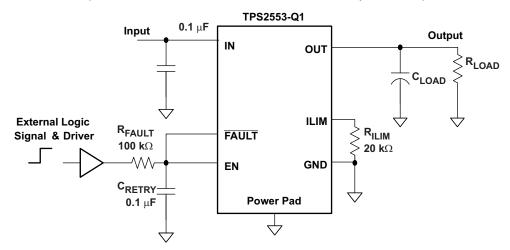


Figure 26. Auto-Retry Functionality With External EN Signal



#### TWO-LEVEL CURRENT-LIMIT CIRCUIT

Some applications require different current-limit thresholds depending on external system conditions. Figure 27 shows an implementation for an externally controlled, two-level current-limit circuit. The current-limit threshold is set by the total resistance from ILIM to GND (see the Programming the Current-Limit Threshold section). A logic-level input enables/disables MOSFET Q1 and changes the current-limit threshold by modifying the total resistance from ILIM to GND. Additional MOSFET/resistor combinations can be used in parallel to Q1/R2 to increase the number of additional current-limit levels.

#### **NOTE**

ILIM should never be driven directly with an external signal.

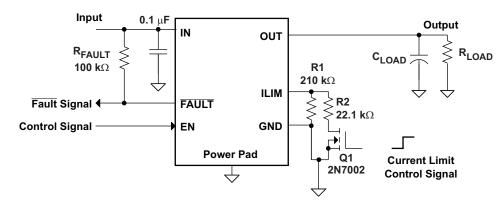


Figure 27. Two-Level Current-Limit Circuit

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#### PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing		Package Qty	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Top-Side Markings	Samples
TPS2553QDBVRQ1	ACTIVE	SOT-23	DBV	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR		PYEQ	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

<sup>(4)</sup> Only one of markings shown within the brackets will appear on the physical device.

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#### OTHER QUALIFIED VERSIONS OF TPS2553-Q1:

Catalog: TPS2553

NOTE: Qualified Version Definitions:





24-Jan-2013

• Catalog - TI's standard catalog product

# PACKAGE MATERIALS INFORMATION

www.ti.com 5-Dec-2012

## TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

## QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

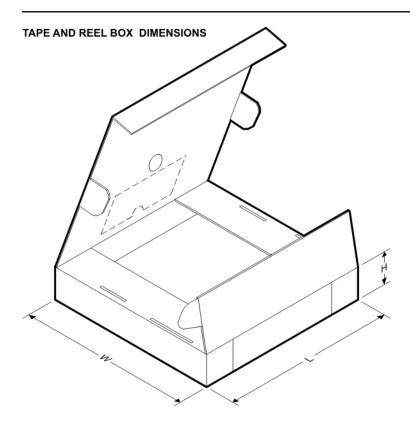


### \*All dimensions are nominal

Device	Package Type	Package Drawing			Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS2553QDBVRQ1	SOT-23	DBV	6	3000	178.0	9.0	3.23	3.17	1.37	4.0	8.0	Q3

**PACKAGE MATERIALS INFORMATION** 

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#### \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS2553QDBVRQ1	SOT-23	DBV	6	3000	180.0	180.0	18.0

# DBV (R-PDSO-G6)

# PLASTIC SMALL-OUTLINE PACKAGE



NOTES:

- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.15 per side.
- D. Leads 1,2,3 may be wider than leads 4,5,6 for package orientation.
- Falls within JEDEC MO-178 Variation AB, except minimum lead width.



# DBV (R-PDSO-G6)

# PLASTIC SMALL OUTLINE



NOTES:

- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
- D. Publication IPC-7351 is recommended for alternate designs.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.



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