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# 3A High Efficient Synchronous Step Down Converter with DCS<sup>™</sup> Control

Check for Samples: TLV62090

## FEATURES

- 2.5 V to 5.5 V Input Voltage Range
- DCS<sup>™</sup> Control
- 95% Converter Efficiency
- Power Save Mode
- 20 µA Operating Quiescent Current
- 100% Duty Cycle for Lowest Dropout
- 1.4 MHz Typical Switching Frequency
- 0.8 V to V<sub>IN</sub> Adjustable Output Voltage
- Output Discharge Function
- Adjustable Softstart
- Two Level Short Circuit Protection
- Output Voltage Tracking
- Wide Output Capacitance Selection
- Available in 3x3mm 16 Pin QFN Package

L1 1μΗ

C4 OnF R1

200k

R2

R3 500k

# **APPLICATIONS**

- Distributed Power Supplies
- Notebook, Netbook Computers
- Hard Disk Drivers
- Processor Supply

C1

22µF

Vin

2.5V to 5.5V O

Battery Powered Applications

TLV62090

sw

sw

vos

FB

PG

SS

AGND

PGND PGND

PVIN

PVIN

AVIN

DEF

ΕN

СР

CN

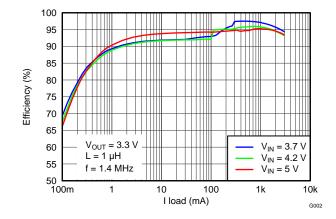
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10nF

# DESCRIPTION

The TLV62090 device is a high frequency synchronous step down converter optimized for small solution size, high efficiency and suitable for battery powered applications. To maximize efficiency, the converter operates in PWM mode with a nominal switching frequency of 1.4 MHz and automatically enters Power Save Mode operation at light load currents. When used in distributed power supplies and point of load regulation, the device allows voltage tracking to other voltage rails and tolerates output capacitors ranging from 10  $\mu$ F up to 150  $\mu$ F and beyond. Using the DCS<sup>TM</sup> Control topology the device achieves excellent load transient performance and accurate output voltage regulation.

The output voltage start-up ramp is controlled by the softstart pin, which allows operation as either a standalone power supply or in tracking configurations. Power sequencing is also possible by configuring the Enable and Power Good pins. In Power Save Mode, the device operates at typically 20  $\mu$ A quiescent current. Power Save Mode is entered automatically and seamlessly maintaining high efficiency over the entire load current range.



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Vout

1.8V/3A

o

-0

Power Good



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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

#### ORDERING INFORMATION<sup>(1)</sup>

T <sub>A</sub>	ORDERING	PACKAGE	PACKAGE MARKING
-40°C to 85°C	TLV62090	RGT	SBV

 For detailed ordering information please see the PACKAGE OPTION ADDENDUM section at the end of the datasheet.

### ABSOLUTE MAXIMUM RATINGS<sup>(1)</sup>

over operating free-air temperature range (unless otherwise noted)

		VALUE		
		MIN	MAX	UNIT
Valtara ranza	PVIN, AVIN, FB, SS, EN, DEF, VOS <sup>(2)</sup>	-0.3	7	V
Voltage range	SW, PG	-0.3	V <sub>IN</sub> +0.3	V
Power Good sink current	PG		1	mA
ESD ration	Human Body Model		2	kV
ESD rating	Charged Device Model		500	V
Continuous total power dissip	pation	See the Thermal Table		
Operating junction temperatu	re range, T <sub>J</sub>	-40	150	°C
Operating ambient temperatu	ire range, T <sub>A</sub>	-40	85	°C
Storage temperature range, 7	Tstg	-65	150	°C

(1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltage values are with respect to network ground terminal.

#### THERMAL INFORMATION

	THERMAL METRIC <sup>(1)</sup>	TPS62090		
		QFN (16 PINS)	UNITS	
$\theta_{JA}$	Junction-to-ambient thermal resistance	47		
$\theta_{JCtop}$	Junction-to-case (top) thermal resistance	60		
$\theta_{JB}$	Junction-to-board thermal resistance	20	°C/W	
$\Psi_{JT}$	Junction-to-top characterization parameter	1.5	C/W	
$\Psi_{JB}$	Junction-to-board characterization parameter	20		
$\theta_{\text{JCbot}}$	Junction-to-case (bottom) thermal resistance	5.3		

(1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, SPRA953. **RECOMMENDED OPERATING CONDITIONS**<sup>(1)</sup>

		MIN	TYP MAX	UNIT
V <sub>IN</sub>	Input voltage range V <sub>IN</sub>	2.5	5.5	V
T <sub>A</sub>	Operating ambient temperature	-40	85	°C
TJ	Operating junction temperature	-40	125	°C

(1) See the application section for further information



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## **ELECTRICAL CHARACTERISTICS**

 $V_{IN}$  = 3.6V,  $T_A$  = -40°C to 85°C, typical values are at  $T_A$  = 25°C (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPL	Y					
V <sub>IN</sub>	Input voltage range		2.5		5.5	V
I <sub>QIN</sub>	Quiescent current	Not switching, FB = FB +5 %, Into PVIN and AVIN		20		μA
I <sub>sd</sub>	Shutdown current	Into PVIN and AVIN		0.6	5	μA
	Undervoltage lockout threshold	V <sub>IN</sub> falling	2.1	2.2	2.3	V
UVLO	Undervoltage lockout hysteresis			200		mV
	Thermal shutdown	Temperature rising		150		°C
	Thermal shutdown hysteresis			20		°C
Control	SIGNAL EN	·				
V <sub>H</sub>	High level input voltage	V <sub>IN</sub> = 2.5 V to 6 V	1			V
VL	Low level input voltage	V <sub>IN</sub> = 2.5 V to 6 V			0.4	V
l <sub>lkg</sub>	Input leakage current	$EN = GND \text{ or } V_{IN}$		10	100	nA
R <sub>PD</sub>	Pull down resistance			400		kΩ
Softsta	rt	·			L	
I <sub>SS</sub>	Softstart current		6.3	7.5	8.7	μA
POWER	R GOOD	·			L	
.,	Power good threshold	Output voltage rising		95%		
V <sub>th</sub>		Output voltage falling		90%		
VL	Low level voltage	I <sub>(sink)</sub> = 1mA			0.4	V
I <sub>PG</sub>	PG sinking current				1	mA
I <sub>lkg</sub>	Leakage current	V <sub>PG</sub> = 3.6V		10	100	nA
	RSWITCH	ł			ŀ	
_	High side FET on-resistance	I <sub>SW</sub> = 500 mA		50		mΩ
R <sub>DS(on)</sub>	Low side FET on-resistance	I <sub>SW</sub> = 500 mA		40		mΩ
I <sub>LIM</sub>	High side FET switch current limit		3.7	4.6	5.5	А
f <sub>s</sub>	Switching frequency	I <sub>OUT</sub> = 3 A		1.4		MHz
OUTPU	T	+ · · ·				
Vs	Output voltage range		0.8		V <sub>IN</sub>	V
R <sub>od</sub>	Output discharge resistor	EN = GND, V <sub>OUT</sub> = 1.8 V		200		Ω
V <sub>FB</sub>	Feedback regulation voltage			0.8		V
10		$V_{IN} \ge V_{OUT} + 1 V$ , TPS62090 adjustable output version				
	Feedback voltage	I <sub>OUT</sub> = 1 A, PWM mode	-1.4%		+1.4%	
V <sub>FB</sub>	accuracy <sup>(1)</sup> <sup>(2)</sup>	$I_{OUT} = 0 \text{ mA}, V_{OUT} \ge 1.2 \text{ V}, \text{ PFM mode}$	-1.4%		+3%	
		$I_{OUT} = 0$ mA, $V_{OUT} < 1.2V$ , PFM mode	-1.4%		+3.7%	
I <sub>FB</sub>	Feedback input bias current	$V_{FB} = 0.8V$ , TPS62090 adjustable output version		10	100	nA
0	Line regulation	V <sub>OUT</sub> = 1.8 V, PWM operation		0.016		%/V
	Load regulation	$V_{OUT} = 1.8 \text{ V}, \text{PWM operation}$		0.04		%/A

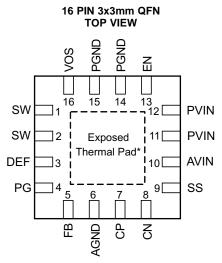
(1) For output voltages < 1.2 V, use a 2 x 22  $\mu$ F output capacitance to achieve +3% output voltage accuracy in PFM mode. (2) Conditions: L = 1  $\mu$ H, C<sub>OUT</sub> = 22  $\mu$ F. For more information, see the Power Save Mode Operation section of this data sheet.

TEXAS INSTRUMENTS

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## **DEVICE INFORMATION**



NOTE: \*The exposed Thermal Pad is connected to AGND.

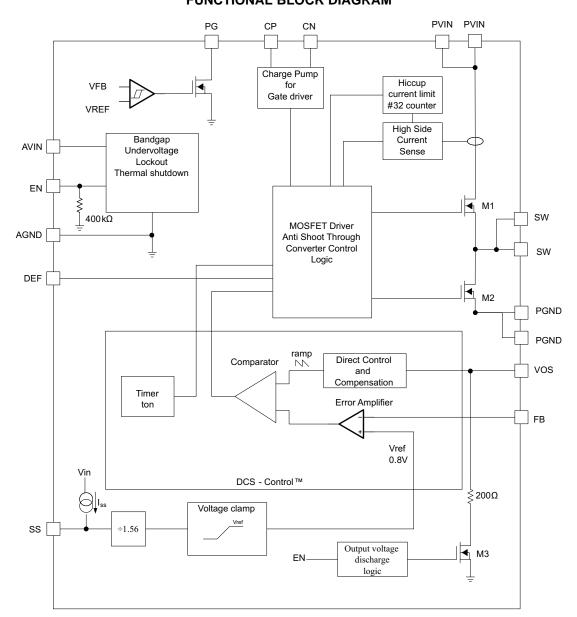
#### PIN FUNCTIONS

PIN		I/O	DESCRIPTION		
NAME	NO.	1/0	DESCRIPTION		
SW	1, 2	Ι	Switch pin of the power stage.		
DEF	3	Ι	This pin is used for internal logic and needs to be pulled high. This pin should not be left floating.		
PG	4	0	Power good open drain output. This pin is high impedance if the output voltage is within regulation. This pin is pulled low if the output is below its nominal value. The pull up resistor can not be connected to any voltage higher than the input voltage of the device.		
FB	5		Feedback pin of the device.		
AGND	6		Analog ground.		
CP	7		Internal charge pump flying capacitor. Connect a 10 nF capacitor between CP and CN.		
CN	8		Internal charge pump flying capacitor. Connect a 10 nF capacitor between CP and CN.		
SS	9	I	Soft-start control pin. A capacitor is connected to this pin and sets the softstart time. Leaving this pin floating sets the minimum start-up time.		
AVIN	10		Bias supply input voltage pin.		
PVIN	11,12		Power supply input voltage pin.		
EN 13			Device enable. To enable the device this pin needs to be pulled high. Pulling this pin low disables the device. This pin has an active pull down resistor of typically 400 k $\Omega$ .		
PGND	14,15		Power ground connection.		
VOS	16		Output voltage sense pin. This pin needs to be connected to the output voltage.		
Thermal Pa	ld		The exposed thermal pad is connected to AGND.		



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# FUNCTIONAL BLOCK DIAGRAM



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	Table 1. List of components						
REFERENCE	REFERENCE DESCRIPTION MANUFACTURER						
TLV62090	High efficient step down converter	Texas Instruments					
L1	Inductor: 1uH	Coilcraft XFL4020-102					
C1	C1 Ceramic capacitor: 22uF (6.3)						
C2	Ceramic capacitor: 22uF	(6.3V, X5R, 0805)					
C3, C4	C3, C4 Ceramic capacitor Standard						
R1, R2, R3	Resistor	Standard					

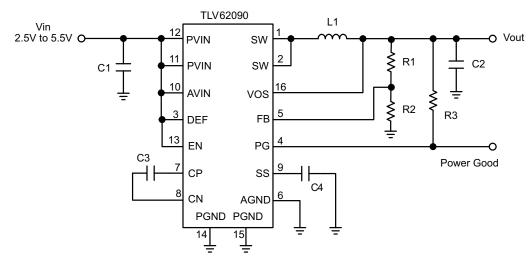


Figure 1. Parametric Measurement Circuit

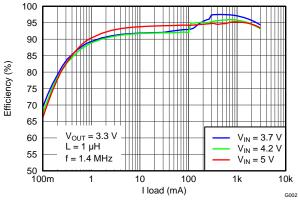


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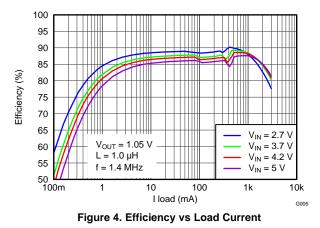
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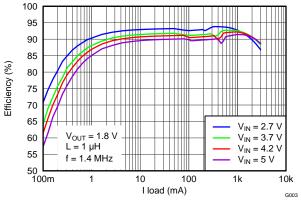
# **TYPICAL CHARACTERISTICS**

		FIGURE
Efficiency	vs load current ( $V_0 = 3.3 V$ )	Figure 2
Efficiency	vs load current ( $V_0 = 1.8 V$ )	Figure 3
Efficiency	vs load current ( $V_0 = 1.05 V$ )	Figure 4
Output voltage	vs load current ( $V_0 = 1.8 V$ )	Figure 5
High Side FET on-resistance	vs input voltage	Figure 6
Switching frequency	vs load current ( $V_0 = 1.8 V$ )	Figure 7
Switching frequency	vs input voltage (V <sub>O</sub> = 1.8 V)	Figure 8
Quiescent current	vs input voltage ( $V_O = 1.8 V$ )	Figure 9
PWM operation	V <sub>O</sub> = 1.8 V	Figure 10
PFM operation	V <sub>O</sub> = 1.8 V	Figure 11
Load sweep	V <sub>O</sub> = 1.8 V	Figure 12
Start-up	V <sub>O</sub> = 1.8 V, C <sub>SS</sub> = 10 nF	Figure 13
Shutdown	V <sub>O</sub> = 1.8 V	Figure 14
Hiccup short circuit protection	V <sub>O</sub> = 1.8 V	Figure 15
Hiccup Short circuit protection	$V_{O}$ = 1.8 V, recovery after short circuit	Figure 16
Load transient response	V <sub>O</sub> = 1.8 V, 300 mA to 2.5 A	Figure 17
Load transient response	V <sub>O</sub> = 1.8 V, 300 mA to 2.5 A	Figure 18
Load transient response	V <sub>O</sub> = 1.8 V, 20 mA to 1 A	Figure 19

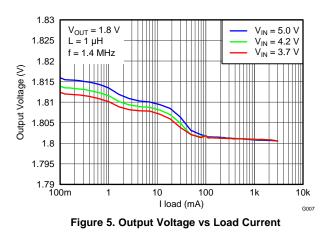














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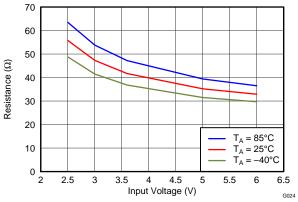


Figure 6. High Side FET On-Resistance vs Input Voltage

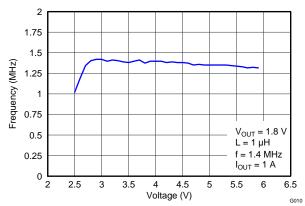
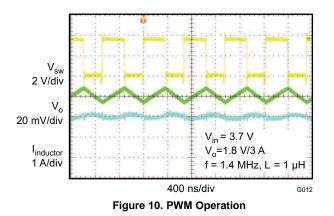


Figure 8. Switching Frequency vs Input Voltage



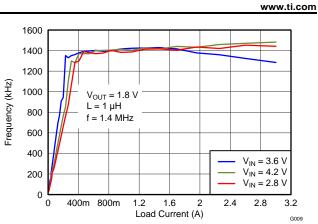


Figure 7. Switching Frequency vs Load Current

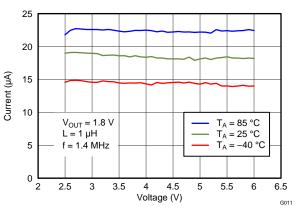


Figure 9. Quiescent Current vs Input Voltage

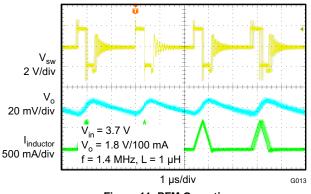
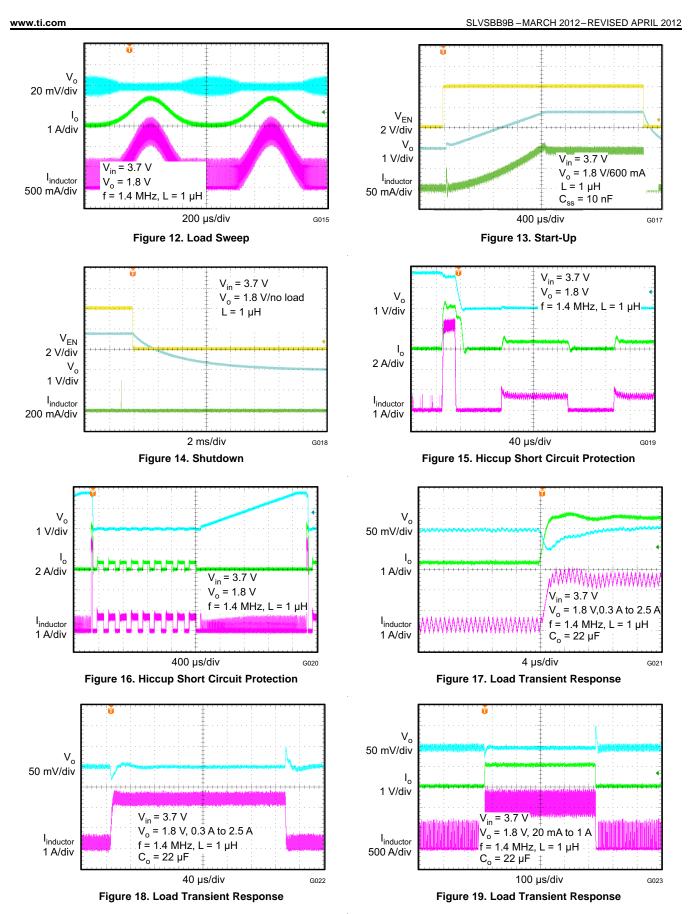


Figure 11. PFM Operation





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## DETAILED DESCRIPTION

#### Operation

The TLV62090 synchronous switched mode converter is based on DCS<sup>™</sup> Control (Direct Control with Seamless transition into Power Save Mode). This is an advanced regulation topology that combines the advantages of hysteretic and voltage mode control.

The DCS<sup>™</sup> Control topology operates in PWM (Pulse Width Modulation) mode for medium to heavy load conditions and in Power Save Mode at light load currents. In PWM, the converter operates with its nominal switching frequency of 1.4 MHz having a controlled frequency variation over the input voltage range. As the load current decreases, the converter enters Power Save Mode, reducing the switching frequency and minimizing the IC quiescent current to achieve high efficiency over the entire load current range. DCS<sup>™</sup> Control supports both operation modes (PWM and PFM) using a single building block having a seamless transition from PWM to Power Save Mode without effects on the output voltage. The TLV62090 offers excellent DC voltage regulation and load transient regulation, combined with low output voltage ripple, minimizing interference with RF circuits.

#### **PWM Operation**

٠*،* 

At medium to heavy load currents, the device operates with pulse width modulation (PWM) at a nominal switching frequency of 1.4 MHz. As the load current decreases, the converter enters the Power Save Mode operation reducing its switching frequency. The device enters Power Save Mode at the boundary to discontinuous conduction mode (DCM).

#### Power Save Mode Operation

As the load current decreases, the converter enters Power Save Mode operation. During Power Save Mode the converter operates with reduced switching frequency in PFM mode and with a minimum quiescent current while maintaining high efficiency. The Power Save Mode is based on a fixed on-time architecture following Equation 1.

$$ton = \frac{\frac{V_{OUT}}{V_{IN}} \times 360 \text{ ns} \times 2}{f} = \frac{2 \times I_{OUT}}{ton^2 \left(1 + \frac{V_{IN} - V_{OUT}}{V_{OUT}}\right) \times \frac{V_{IN} - V_{OUT}}{L}}$$

(1)

In Power Save Mode the output voltage rises slightly above the nominal output voltage in PWM mode, as shown in Figure 5. This effect can be reduced by increasing the output capacitance or the inductor value. This effect can also be reduced by programming the output voltage of the TLV62090 lower than the target value. As an example, if the target output voltage is 3.3 V, then the TLV62090 can be programmed to 3.3V - 0.8%. As a result the output voltage accuracy is now -2.2% to +2.2% instead of -1.4% to 3%. The output voltage accuracy in PFM operation is reflected in the electrical specification table and given for a 22  $\mu$ F output capacitance.

#### Low Dropout Operation (100% Duty Cycle)

The device offers low input to output voltage difference by entering 100% duty cycle mode. In this mode the high side MOSFET switch is constantly turned on. This is particularly useful in battery powered applications to achieve longest operation time by taking full advantage of the whole battery voltage range. The minimum input voltage where the output voltage falls below its nominal regulation value is given by:

$$V_{\rm IN(min)} = V_{\rm OUT(max)} + I_{\rm OUT} x (R_{\rm DS(on)} + R_{\rm L})$$

(2)



#### Where

R<sub>DS(on)</sub> = High side FET on-resistance

 $R_L = DC$  resistance of the inductor

V<sub>OUT(max)</sub> = nominal output voltage plus maximum output voltage tolerance

## Softstart (SS)

To minimize inrush current during start up, the device has an adjustable softstart depending on the capacitor value connected to the SS pin. The device charges the softstart capacitor with a constant current of typically 7.5  $\mu$ A. The feedback voltage follows this voltage with a fraction of 1.56 until the internal reference voltage of 0.8 V is reached. The softstart operation is completed once the voltage at the softstart capacitor has reached typically 1.25 V. The soft-start time can be calculated using Equation 3. The larger the softstart capacitor the longer the softstart time. The relation between softstart voltage and feedback voltage can be estimated using Equation 4.

$$t_{SS} = C_{SS} \times \frac{1.25V}{7.5\mu A}$$

$$V_{FB} = \frac{V_{SS}}{1.56}$$
(3)

This is also the case for the fixed output voltage option having the internal regulation voltage. Leaving the softstart pin floating sets the minimum start-up time.

#### Start-up Tracking (SS)

The softstart pin can also be used to implement output voltage tracking with other supply rails. The internal reference voltage follows the voltage at the softstart pin with a fraction of 1.56 until the internal reference voltage of 0.8 V is reached. The softstart pin can be used to implement output voltage tracking as shown in Figure 20.

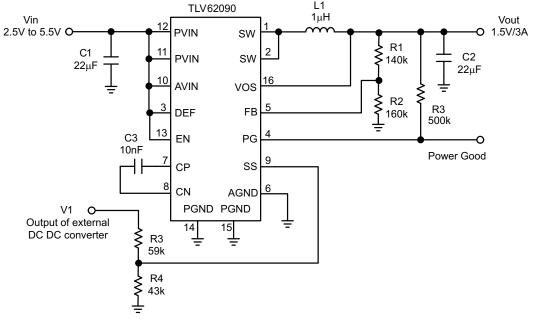


Figure 20. Output Voltage Tracking

In Figure 20, the output V2 tracks the voltage applied to V1. The voltage tracks simultaneously when following conditions are met:

$$\frac{R3}{R4} = \frac{R1}{R2} \times 1.56$$

(5)

As the fraction of R3/R4 becomes larger the voltage V1 ramps up faster than V2, and if it gets smaller then the ramp is slower than V2. R4 needs to be determined first using Equation 6.



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$$R4 = \frac{1.25V}{300\mu A}$$

(6)

In the calculation of R4, 300  $\mu$ A current is used to achieve sufficient accuracy by taking into account the typical 7.5  $\mu$ A soft-start current. After determining R4, R3 can be calculated using Equation 5.

## Short Circuit Protection (Hiccup-Mode)

The device is protected against hard short circuits to GND and over-current events. This is implemented by a two level short circuit protection. During start-up and when the output is shorted to GND the switch current limit is reduced to 1/3 of its typical current limit of 4.6 A. Once the output voltage exceeds typically 0.6 V the current limit is released to its nominal value. The full current limit is implemented as a hiccup current limit. Once the internal current limits is triggered 32 times the device stops switching and starts a new start-up sequence after a typical delay time of 66  $\mu$ S passed by. The device will go through these cycles until the high current condition is released.

#### **Output Discharge Function**

To make sure the device starts up under defined conditions, the output gets discharged via the VOS pin with a typical discharge resistor of 200  $\Omega$  whenever the device shuts down. This happens when the device is disabled or if thermal shutdown, undervoltage lockout or short circuit hiccup-mode is triggered.

### Power Good Output (PG)

The power good output is low when the output voltage is below its nominal value. The power good will become high impedance once the output is within 5% of regulation. The PG pin is an open drain output and is specified to typically sink up to 1 mA. This output requires a pull-up resistor to be monitored properly. The pull-up resistor cannot be connected to any voltage higher than the input voltage of the device.

#### Undervoltage Lockout (UVLO)

To avoid mis-operation of the device at low input voltages, an undervoltage lockout is included. UVLO shuts down the device at input voltages lower than typically 2.2 V with a 200 mV hysteresis.

#### Thermal Shutdown

The device goes into thermal shutdown once the junction temperature exceeds typically 150°C with a 20°C hysteresis.



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#### **APPLICATION INFORMATION**

#### **DESIGN PROCEDURE**

The first step is the selection of the output filter components. To simplify this process, and Table 2 outline possible inductor and capacitor value combinations.

INDUCTOR VALUE [µH] <sup>(1)</sup>	OUTPUT CAPACITOR VALUE [µF] <sup>(2)</sup>					
	10	22	47	100	150	
0.47		$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	
1.0	$\checkmark$	√(3)	$\checkmark$	$\checkmark$	$\checkmark$	
2.2	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	
3.3						

Table 2. Output Filter Sele	ection
-----------------------------	--------

(1) Inductor tolerance and current de-rating is anticipated. The effective inductance can vary by +20% and -30%.

(2) Capacitance tolerance and bias voltage de-rating is anticipated. The effective capacitance can vary by +20% and -50%.

(3) Typical application configuration. Other check mark indicates alternative filter combinations

#### **Inductor Selection**

The inductor selection is affected by several parameter like inductor ripple current, output voltage ripple, transition point into Power Save Mode, and efficiency. See Table 3 for typical inductors.

INDUCTOR VALUE COMPONENT SUPPLIER SIZE (LxWxH mm) Isat/DCR								
0.6 µH	Coilcraft XAL4012-601	4 x 4 x 2.1	7.1A/9.5 mΩ					
1 µH	Coilcraft XAL4020-102	4 x 4 x 2.1	5.9A/13.2 mΩ					
1 µH	Coilcraft XFL4020-102	4 x 4 x 2.1	5.1 A/10.8 mΩ					
0.47 µH	TOKO DFE252012 R47	2.5 x 2 x 1.2	3.7A/39 mΩ					
1 µH	TOKO DFE252012 1R0	2.5 x 2 x 1.2	3.0A/59 mΩ					
0.68 µH	TOKO DFE322512 R68	3.2 x 2.5 x 1.2	3.5A/37 mΩ					
1 µH	TOKO DFE322512 1R0	3.2 x 2.5 x 1.2	3.1A/45 mΩ					

#### **Table 3. Inductor Selection**

In addition, the inductor has to be rated for the appropriate saturation current and DC resistance (DCR). The inductor needs to be rated for a saturation current as high as the typical switch current limit, of 4.6 A or according to Equation 7 and Equation 8. Equation 7 and Equation 8 calculate the maximum inductor current under static load conditions. The formula takes the converter efficiency into account. The converter efficiency can be taken from the data sheet graph's or 80% can be used as a conservative approach. The calculation must be done for the maximum input voltage where the peak switch current is highest.

$$I_{L} = I_{OUT} + \frac{\Delta I_{L}}{2}$$

$$I_{L} = I_{OUT} + \frac{\frac{V_{OUT}}{\eta} \times \left(1 - \frac{V_{OUT}}{V_{IN} \times \eta}\right)}{2 \times f \times L}$$

where

f = Converter switching frequency (typical 1.4 MHz)

L = Selected inductor value

 $\eta$  = Estimated converter efficiency (use the number from the efficiency curves or 0.80 as an conservative assumption)

**Note:** The calculation must be done for the maximum input voltage of the application

Calculating the maximum inductor current using the actual operating conditions gives the minimum saturation current. A margin of 20% needs to be added to cover for load transients during operation.

(7)

(8)



#### Input and Output Capacitor Selection

For best output and input voltage filtering, low ESR ceramic capacitors are recommended. The input capacitor minimizes input voltage ripple, suppresses input voltage spikes and provides a stable system rail for the device. A 22  $\mu$ F or larger input capacitor is recommended. The output capacitor value can range from 10  $\mu$ F up to 150  $\mu$ F and beyond. The recommended typical output capacitor value is 22  $\mu$ F and can vary over a wide range as outline in the output filter selection table.

## Setting the Output Voltage

The output voltage is set by an external resistor divider according to the following equations:

$$V_{OUT} = V_{FB} \times \left(1 + \frac{R1}{R2}\right) = 0.8 \text{ V} \times \left(1 + \frac{R1}{R2}\right)$$
(9)

$$R2 = \frac{V_{FB}}{I_{FB}} = \frac{0.8 V}{5 \mu A} \approx 160 k\Omega$$
(10)

$$R1 = R2 \times \left(\frac{V_{OUT}}{V_{FB}} - 1\right) = R2 \times \left(\frac{V_{OUT}}{0.8V} - 1\right)$$
(11)

When sizing R2, in order to achieve low quiescent current and acceptable noise sensitivity, use a minimum of 5  $\mu$ A for the feedback current I<sub>FB</sub>. Larger currents through R2 improve noise sensitivity and output voltage accuracy.

#### Layout Guideline

It is recommended to place all components as close as possible to the IC. The VOS connection is noise sensitive and needs to be routed as short and directly to the output terminal of the inductor. The exposed thermal pad of the package, analog ground (pin 6) and power ground (pin 14, 15) should have a single joint connection at the exposed thermal pad of the package. This minimizes switch node jitter. The charge pump capacitor connected to CP and CN should be placed close to the IC to minimize coupling of switching waveforms into other traces and circuits. See the evaluation module User Guide (SLVU670) for an example of component placement, routing and thermal design.

### **TYPICAL APPLICATIONS**

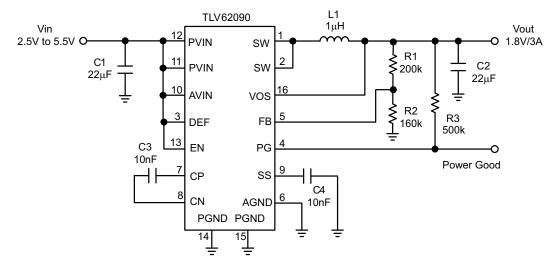
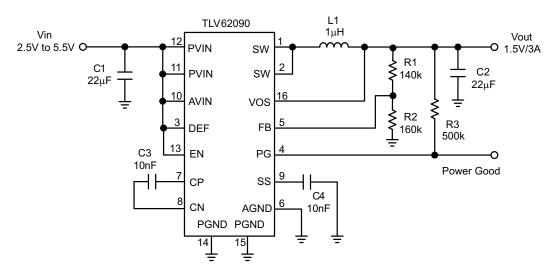


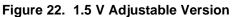
Figure 21. 1.8 V Adjustable Version



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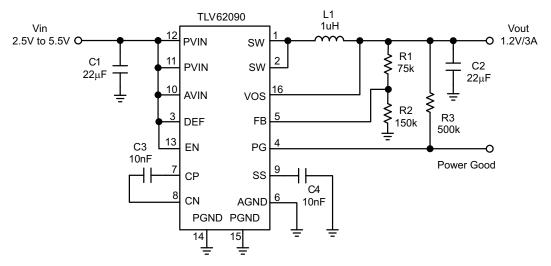
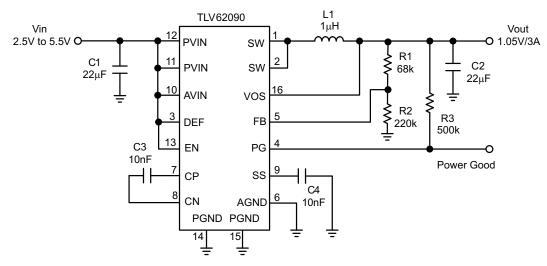


Figure 23. 1.2 V Adjustable Version



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## **REVISION HISTORY**

Cł	nanges from Original (March 2012) to Revision A	Page
•	Changed Vin From: 2.5V to 6V To: 2.5V to 5.5V in Figure 1	6
•	Changed Vin From: 2.5V to 6V To: 2.5V to 5.5V in Figure 20	11
•	Changed Vin From: 2.5V to 6V To: 2.5V to 5.5V in Figure 21, Figure 22, Figure 23, and Figure 24	14
Cł	nanges from Revision A (March 2012) to Revision B	Page

• C	anged the Input voltage range MAX value From: 6V To 5.5V	3
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11-Apr-2013

## **PACKAGING INFORMATION**

Orderable Device	Status	Package Type	Package	Pins	Package	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Top-Side Markings	Samples
	(1)		Drawing		Qty	(2)		(3)		(4)	
TLV62090RGTR	ACTIVE	QFN	RGT	16	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 85	SBV	Samples
TLV62090RGTT	ACTIVE	QFN	RGT	16	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 85	SBV	Samples

<sup>(1)</sup> The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes. **Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between

the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

<sup>(3)</sup> MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) Multiple Top-Side Markings will be inside parentheses. Only one Top-Side Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Top-Side Marking for that device.

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# PACKAGE MATERIALS INFORMATION

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## TAPE AND REEL INFORMATION





# QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal												
Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TLV62090RGTR	QFN	RGT	16	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TLV62090RGTT	QFN	RGT	16	250	180.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2

TEXAS INSTRUMENTS

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# PACKAGE MATERIALS INFORMATION

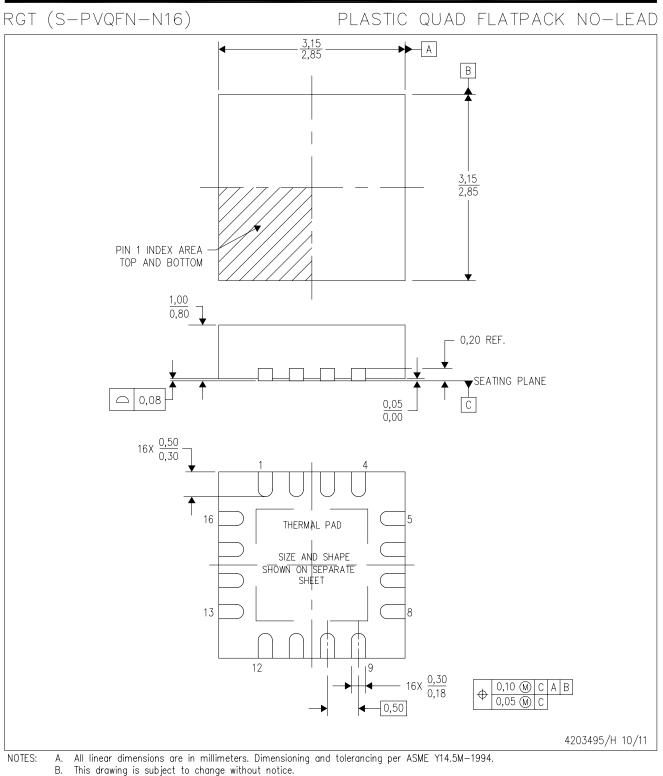
5-Jun-2013



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TLV62090RGTR	QFN	RGT	16	3000	367.0	367.0	35.0
TLV62090RGTT	QFN	RGT	16	250	210.0	185.0	35.0

# **MECHANICAL DATA**



- Quad Flatpack, No-leads (QFN) package configuration. C. D.
- The package thermal pad must be soldered to the board for thermal and mechanical performance. E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions.
- F. Falls within JEDEC MO-220.



# RGT (S-PVQFN-N16)

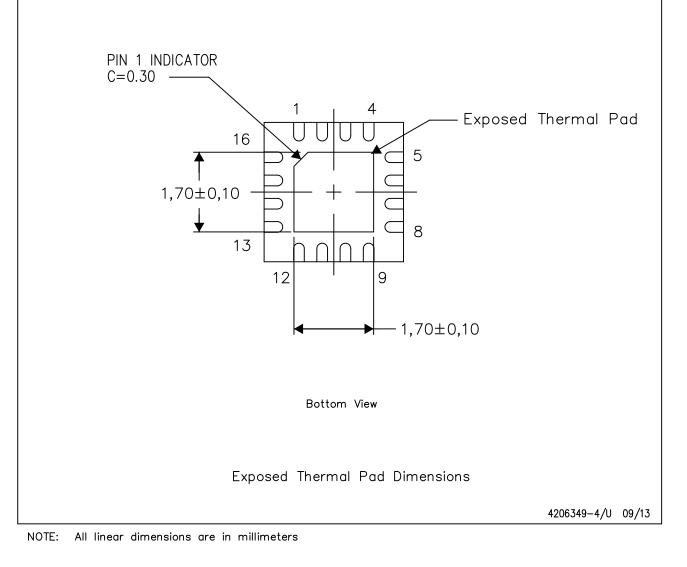
## PLASTIC QUAD FLATPACK NO-LEAD

#### THERMAL INFORMATION

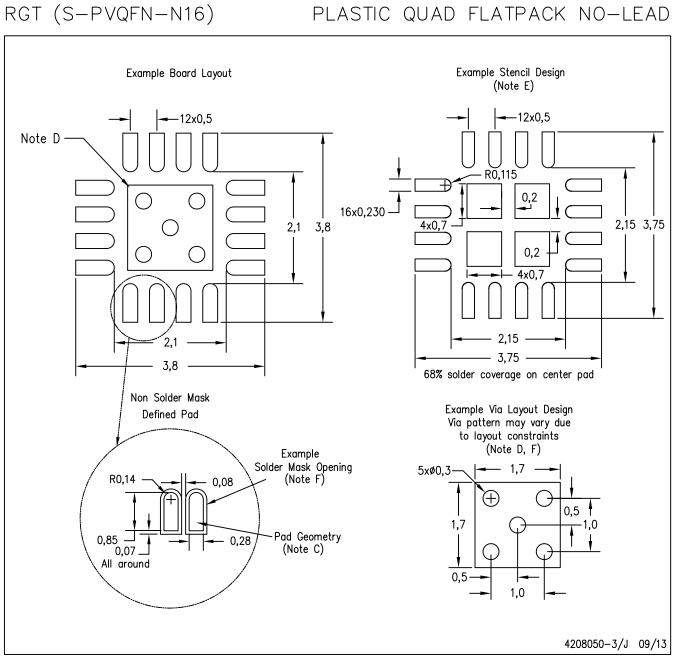
This package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For information on the Quad Flatpack No-Lead (QFN) package and its advantages, refer to Application Report, QFN/SON PCB Attachment, Texas Instruments Literature No. SLUA271. This document is available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.







- NOTES: A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Publication IPC-7351 is recommended for alternate designs.
  - D. This package is designed to be soldered to a thermal pad on the board. Refer to Application Note, QFN/SON PCB Attachment, Texas Instruments Literature No. SLUA271, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <http://www.ti.com>.
  - E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC 7525 for stencil design considerations.
  - F. Customers should contact their board fabrication site for minimum solder mask web tolerances between signal pads.



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